



|| Jai Sri Gurudev ||  
**S J C Institute of Technology, Chickballapur**  
**Department of Civil Engineering**  
**CO-PO and CO-PSO Mapping**

Name of the Faculty: Mr. Ravindranath.C and Ms. Ankitha. V

Subject: Fluid Mechanics Sub code: 17CV33

Semester: III

**Course Objectives:**

The objectives of this course are to make students learn:

1. The Fundamental properties of fluids and its applications.
2. Hydrostatic laws and application to practical problem solving
3. Principles of Kinematics and Hydro-Dynamics for practical applications
4. Basic design of pipes and pipe networks considering flow, pressure and its losses.
5. The basic flow rate measurements.

**Course Outcomes:**

After studying this course, students will be able to:

<b>CO1</b>	Apply a sound knowledge of fundamental properties of fluids and fluid Continuum
<b>CO2</b>	Analyzing solve problems on hydrostatics, including practical applications
<b>CO3</b>	Analyze principles of mathematics to represent kinematic concepts related to fluid flow
<b>CO4</b>	Apply fundamental laws of fluid mechanics and the Bernoulli's principle for practical applications
<b>CO5</b>	Evaluating the discharge through pipes and over notches and weirs

**Programme Specific Outcomes (PSO's)**

After Successful completion of B.E programme in Civil Engineering, the students will be able to:

**PSO1:** Apply Civil Engineering knowledge in analysis, design, laboratory investigations and construction aspects.

**PSO2:** Solve problems in various fields of Civil Engineering with appropriate construction materials and technology.

CO-PO Mapping													CO-PSO Mapping	
	PO1	PO2	PO3	PO4	PO5	PO6	PO7	PO8	PO9	PO10	PO11	PO12	PSO1	PSO2
CO1	2	1	1	-	-	-	-	1	-	-	-	-	2	1
CO2	2	2	2	-	-	-	2	1	-	-	-	-	1	2
CO3	2	2	1	-	-	-	-	1	-	-	-	-	1	2
CO4	1	1	2	-	-	-	2	1	-	-	-	-	2	1
CO5	1	1	3	-	-	-	-	1	-	-	-	-	1	2
Avg	1.6	1.4	1.8	-	-	-	-	2	1	-	-	-	3	1
1: Slightly      2: Moderately      3: Substantially													2022/3/14 15:00	

**Justification:**

**CO1:** Apply the knowledge of engineering science in properties of fluid, graduates will able to identify, formulate and analyse the problems in fluid flow and develop appropriate solution.

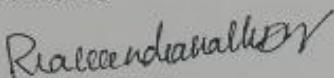
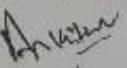
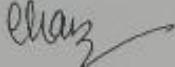
**CO2:** Applying the engineering knowledge of Hydrostatic fluids, analyse the problems and design the solution for complex engineering problems with appropriate solutions in lifelong learning.

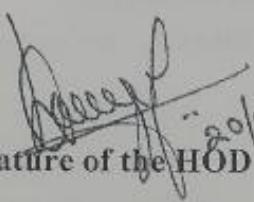
**CO3:** Apply the knowledge of mathematics, engineering fundamentals in the concept of kinematic fluid flow, analyse the problems and develop the solutions with ethical principles in velocity and total acceleration of fluid particles.

**CO4:** Apply the basic engineering knowledge in fundamental laws of fluid mechanics, analyse the problems to develop the solutions and demonstrate the knowledge of Bernoulli's principle for practical applications

**CO5:** Apply the basic engineering knowledge, identify and analyse the problems to design and development the appropriate solutions in discharge through pipes, notches and weirs for the need of lifelong learning with ethical principles.

**Signature of Committee members**

1. Mr. Ravindranath. C 
2. Mrs. Ankitha. V 
3. Mrs. Chandrakala. S 

**Signature of the HOD**  
20/7/2018



Course Title	FLUID MECHANICS					Course Code	C203
Subject Code	17CV33	Semester	3	Section	A & B	Emp.ID	2025
Faculty Name	Mrs. ANKITHA V					No.students	114

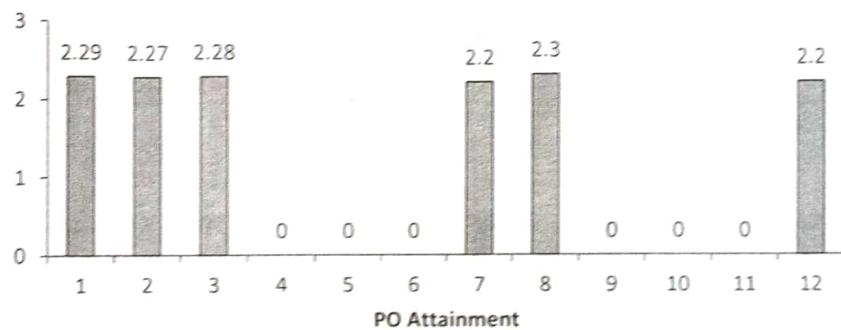
Summary of CO attainments of Sub: 17CV33 Based on (AVERAGE-TYPE-1) Academic Year:2018-19

CO	CID_CO	CIE			SEE			CES			TOT_Attainment		
		S_AT	T_ST	ATN	S_AT	T_ST	ATN	S_AT	T_ST	ATN	ATN	%	Status
CO1	C203.1	340	114	3	218	114	1.9	252	105	2.4	2.4	80	YES
CO2	C203.2	191	101	1.9	218	114	1.9	237	105	2.3	2	65	YES
CO3	C203.3	342	114	3	218	114	1.9	250	105	2.4	2.4	80	YES
CO4	C203.4	336	114	3	218	114	1.9	258	105	2.5	2.4	80	YES
CO5	C203.5	305	114	2.7	218	114	1.9	251	105	2.4	2.3	76	YES

All CO's Attained

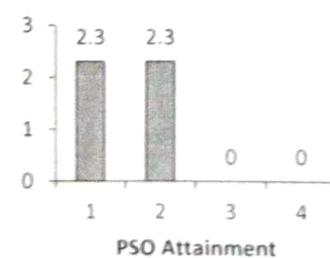
Summary of PO attainments of Sub: 17CV33 Based on (AVERAGE-TYPE-1) Academic Year:2018-19

PO Number	1	2	3	4	5	6	7	8	9	10	11	12
Direct ATNT(D)	2.25	2.23	2.24					2.15	2.27			2.15
Indirect ATNT(ID)	2.39	2.39	2.4					2.4	2.4			2.4
Total-ATNT	2.29	2.27	2.28					2.2	2.3			2.2
ATNT TO SCALE	1.22	1.06	1.37					1.47	1.47			0.77



Summary of PSO attainments in Year:2018-19

PSO Number	1	2	3	4
Direct ATNT(D)	2.26	2.27		
Indirect ATNT(ID)	2.4	2.4		
Total-ATNT	2.3	2.3		
ATNT TO SCALE	1.69	0.77		

Ankitha  
09/05/2019Ankitha  
09/05/2019



## Department : CIVIL ENGINEERING

## LESSON PLAN

CLASS: III SECTION: A	FACULTY: ANKITHA V	SUBJECT: FLUID MECHANICS	SUB CODE: 17CV33
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**OBJECTIVE:** The objectives of this course is to make students to learn:

1. The Fundamental properties of fluids and its applications.
2. Hydrostatic laws and application to practical problem solving.
3. Principles of Kinematics and Hydro-Dynamics for practical applications.
4. Basic design of pipes and pipe networks considering flow, pressure and its losses.
5. The basic flow rate measurements.

**PREREQUISITE(s):** Trigonometry and Elements of civil engineering.

**EXPECTED OUTCOME:** After successful completion of the course, the student will be able to:

1. Possess a sound knowledge of fundamental properties of fluids and fluid continuum.
2. Compute and solve problems on hydrostatics, including practical applications.
3. Apply principles of mathematics to represent kinematic concepts related to fluid flow.
4. Apply fundamental laws of fluid mechanics and the Bernoulli's principle for practical applications.
5. Compute the discharge through pipes and over notches and weirs.

**IT IS BASIC SUBJECT FOR:** Applied Hydraulics and Fluid Mechanics Laboratory

**SUBJECT APPLICATIONS:** Pipe network, discharge measurements

MODULE	TOPIC	PLANNED		ACTUAL		REMARKS
		No of Hours	Date	No of Hours	Date	
1	Fluids & Their Properties: Concept of fluid, Systems of units. Properties of fluid; Mass density, Specific weight, Specific gravity, Specific volume, Viscosity, Cohesion, Adhesion	01	1-8-18	01	02/18	Site visiting
	Surface tension& Capillarity, Fluid as a continuum, Newton's law of viscosity	01	2-8-18	01	03/18	
	Numerical Problems on Viscosity	01	3-8-18	01	06/18	
	Capillary rise in a vertical tube and between two plane surfaces	01	4-8-18	01	08/18	
	Numerical Problems on Capillary	01	6-8-18	01	08/18	
	Vapour pressure of liquid, compressibility and bulk modulus	01	8-8-18	01	09/18	
	Capillarity, surface tension, pressure inside a water droplet, pressure inside a soap bubble and liquid jet	01	9-8-18	01	09/18	
	Numerical problems	01	10-8-18	01	10/18	

	<b>Fluid Pressure and Its Measurements:</b> Definition of pressure, Pressure at a point, Pascal's law.	01	13-8-18	01	13/8	
	Variation of pressure with depth. Types of pressure.	01	16-8-18	01	16/8	
	Measurement of pressure using simple manometers, Numerical problems	01	17-8-18	01	18/8	
	Measurement of pressure using inclined manometers, Numerical problems	01	20-8-18	01	20/8	
	Measurement of pressure using differential manometers, Numerical problems	01	23-8-18	01	23/8	
	Introduction to Mechanical and electronic pressure measuring devices.	01	24-8-18	01	24/8	Xanadu -Lohri festival
	Flip class, Module- 1 Test	01	25-8-18	01	30/8	Link Holiday
2	<b>Hydrostatic forces on Surfaces :</b> Definition, Total pressure, centre of pressure,	01	27-8-18	01	31/8	
	Total pressure on horizontal, vertical and inclined plane surface,	01	29-8-18	01	03/9	
	Total pressure on curved surfaces, water pressure on gravity dams, Lock gates.	01	30-8-18	01	05/9	
	Numerical problems	01	31-8-18	01	05/9	
	<b>Fundamentals of fluid flow (Kinematics):</b> Introduction. Methods of describing fluid motion.	01	1-9-18	01	06/9	
	Velocity and Total acceleration of a fluid particle.	01	3-9-18	01	06/9	
	Tutorial -1	01	5-9-18	01	15/9	
	Types of fluid flow, Description of flow pattern.	01	6-9-18	01	7/9	
	Basic principles of fluid flow, three-dimensional continuity equation in Cartesian coordinate system.	01	7-9-18	02	12/9 14/9	Reptation [14/9]
	<b>1<sup>st</sup> INTERNALS 8-9-18 , 10-9-18, 11-9-18, 12/9/18 to 20/9/18</b>					
	Derivation for Rotational and irrotational motion.	01	12-9-18	01	14/9	
	Potential function, stream function, orthogonality of streamlines and equipotential lines.	01	14-9-18	01	15/9	
	Numerical problems on Stream function and velocity potential.	01	17-9-18	01	17/9	
	Introduction to flow net.	01	19-9-18	01	21/9	
	Flip class, Module 2 Test	01	20-9-18	01	25/9	
3	<b>Fluid Dynamics:</b> Introduction. Forces acting on fluid in motion.	01	22-9-18	01	26/9	

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	Euler's equation of motion along a streamline and Bernoulli's equation	01	24-9-18	01	27/9	
	Assumptions and limitations of Bernoulli's equation. Modified Bernoulli's equation.	01	26-9-18	01	01/10	
	Problems on applications of Bernoulli's equation (with and without losses)	01	27-9-18	01	03/10	
	Vortex motion; forced vortex, free vortex, problems	01	28-9-18	01	04/10	
	Momentum equation problems on pipe bends.	01	29-9-18	01	05/10	
	<b>Applications:</b> Introduction, Venturimeter, Orificemeter, Pitot tube.	01	1-10-18	01	06/10	
	Numerical Problems	01	3-10-18	01	06/10	
	Tutorial - 2	01	4-10-18	01	10/10	
	Flip class, Module- 3 Test	01	5-10-18	01	11/10	
4	<b>Orifice and Mouthpiece:</b> Introduction, classification, flow through orifice	01	6-10-18	01	12/10	
	<b>2<sup>nd</sup> INTERNALS</b> 9-10-18, 10-10-18, 11-10-18				15, 16, 17, 18/10	
	Hydraulic coefficients, Numerical problems.	01	12-10-18	01	22/10	
	Mouthpiece, classification	01	15-10-18	01	25/10	
	Borda's Mouthpiece (No problems).	01	17-10-18	01	31/10	
	<b>Notches and Weirs:</b> Introduction, Classification, discharge over rectangular, Triangular, Trapezoidal notches	01	22-10-18	01	02/11	
	Cippoletti notch, broad crested weirs	01	29-10-18	01	03/11	
	Numerical problems.	01	31-10-18	01	03/11	
	Ventilation of weirs, submerged weirs.	01	2-11-18	01	05/11	
	Tutorial- 3, Module 4 Test	01	3-11-18	01	07/11	
5	<b>Flow through Pipes:</b> Introduction. Major and minor losses in pipe flow.	01	5-11-18	01	14/11	
	Darcy-Weisbach equation for head loss due to friction in a pipe.	01	7-11-18	01	09/11	
	<b>3<sup>rd</sup> INTERNALS</b> 12-11-18, 13-11-18, 14-11-18				22, 23 & 24/11/18	
	Pipes in series, pipes in parallel, equivalent pipe-problems.	01	15-11-18	01	14/11	
	Minor losses in pipe flow, equation for head loss due to sudden expansion.	01	16-11-18	01	19/11	
	Numerical problems.	01	19-11-18	01	16/11	
	Hydraulic gradient line, energy gradient line.	01	22-11-18	01	17/11	
	Pipe Networks, Hardy Cross method	01	23-11-18	01	26/11	
	Numerical problems.	01	24-11-18	01	27/11	
	<b>Surge Analysis in Pipes:</b> Water hammer in pipes	01	26-11-18	01	28/11	



	Equations for pressure rise due to gradual valve closure and sudden closure for rigid and elastic pipes.	01	28-11-18	01	29/11	
	Numerical problems.	01	29-11-18	01	29/11	
	Flip class, Module 5 Test	01	30-11-18	01	30/11	

## Assignments and Mini Project

Assignment - I Submitted on:	24) 9/2018
Assignment - II Submitted on:	22/10/2018
Assignment - III Submitted on: <u>Assignment - IV</u> [Group Assignment] -	22/11/2018 - 28/11/2018

## Literature to be Referred for the Course:

Book Type	Code	Title & Author	Publication Information		
			Edition	Publisher	Year
Text Books	T1	"Hydraulics and Fluid Mechanics", P N Modi and S M Seth.	20 <sup>th</sup>	Standard Book House, New Delhi	2015
	T2	"A Text book of Fluid Mechanics and Hydraulic Machines", R K Bansal.	9 <sup>th</sup>	Laxmi Publications, New Delhi	2005
Reference Books	R1	"Fluid Mechanics", J F Douglas	5 <sup>th</sup>	Pearson	2009

## Comments by Faculty:

Completed as per plan

## Comments by HOD:

*Satisfactory.*

Note: Plan and execution is for 5 Modules.

Prepared by	Mrs. ANKITHA V	Reviewed by	Mr. RAVINDRA M.V	Approved by	Dr. G. NARAYANA
Date & sign	Ankitha V 30/07/18	Date & sign	R. Ravindra M.V 30/07/18	Date & sign	<i>[Signature]</i> 30/07/18

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## Module - 3

①

### Fluid Dynamics

#### Introduction:

Fluid dynamics is a branch of fluid mechanics which deals with the study of fluids under motion along with the forces which induces the motion.

The forces acting on the fluids are known as Hydro-dynamic force. The dynamic law of the fluid motion is obtained by Newton's second law of motion

$$\text{ie., Force} = \text{Mass} \times \text{Acceleration}$$

$$F = m \times a$$

#### Types of forces acting on fluid flow:

For the fluid flow problems the forces acting on the fluid mass may be any one or combination of several of the following forces:-

- 1) Inertia force, ( $F_i$ ) ; & 6) Elastic force ( $F_e$ )
- 2) Vis.ous force ( $F_v$ )
- 3) Gravity force ( $F_g$ )
- 4) Pressure force ( $F_p$ )
- 5) Surface tension force ( $F_s$ )

## Inertia force ( $F_i$ ):-

It is equal to the product of mass & acceleration of the flowing fluid & acts in the direction opposite to the direction of acceleration. It is always existing in fluid flow problem.

$$\text{ie, } F_i = m \times a$$

2) Viscous Force ( $F_v$ ):- It is equal to the product of shear stress ( $\tau$ ) due to viscosity & surface area of the flow. It is present in the fluid flow problems where viscosity is having an important role to play.

$$\text{ie, } F_v = \tau \times A$$

3) Gravity force ( $F_g$ ):- It is equal to the product of mass & acceleration due to gravity of the flowing fluid. It is present in the case of open surface flow.

$$\text{ie, } F_g = m g$$

4) Pressure Force ( $F_p$ ):- It is equal to the product of pressure intensity & C/s area of the flowing fluid. It is present in the case of pipe flow.

$$\text{ie, } F_p = P \times A$$

## Surface tension force ( $F_s$ ):-

②

It is equal to the product of surface tension & length of the surface of the flowing fluid.

$$\text{ie, } F_s = \sigma \times l.$$

6) Elastic force ( $F_e$ ):- It is equal to the product of Elastic stress & area of the flowing fluid.

$$\text{ie, } F_e = k \times A$$

For a flowing fluid, the above mentioned forces may not always be present. And also the forces, which are present in a fluid flow problem, are not of equal magnitude. There are always one or 2 forces which dominate the other forces. These dominant forces govern the flow of fluid.

The problems of fluid mechanics can be solved with the help of the following

3 eqn or laws:-

- 1) Continuity eqn (law of conservation of mass)
- 2) Energy eqn (law of conservation of energy).
- 3) Momentum eqn (law of conservation of momentum or impulse-momentum theory).

## Energy & its forms:-

Energy is defined as the capacity to do work or the capacity to produce the change in existing state. Energy cannot be seen but its effect can be seen & hence it can be completed. Energy is recognized in various forms like potential energy, Kinematic energy, datum energy, chemical energy, electrical energy etc. All these forms are interchangeable.

### Potential Energy:-

It is the energy possessed by the virtue of its position or location w.r.t certain arbitrary datum. Hence, the potential energy represents the work required to move the fluid mass against gravity from the respective position.

$$\begin{aligned} P.E. &= \text{mass} \times \text{acceleration due to gravity} \times \text{height} \\ &= mg \times z \end{aligned}$$

$$\left\{ \begin{array}{l} \text{wt of mass } \times g \\ \text{fluid} = \text{wt} \end{array} \right.$$

$$\begin{aligned} \text{Potential Energy per unit wt} &= \frac{m \times g \times z}{m \times g} = z \end{aligned}$$

Where  $z$  is known as datum head. The datum head may be the (or) +ve depending upon the position of the fluid above or below the reference axis.



The datum head is also termed as potential head.

Kinetic Energy (or) kinetic head or velocity head (or) velocity Energy

The energy possessed by virtue of its motion is termed as kinetic energy or velocity head.

According to Newton's second law of motion we have,

$$F = ma$$

diff w.r.t  $a$

$$\frac{dF}{da} = m$$

$$\therefore dF = m da$$

$$dF = m \cdot \frac{dv}{dt}$$

$\times$  on b.s by  $ds$

$$\therefore dF \times ds = m \cdot \frac{dv}{dt} \times ds$$

{ force  $\times$  distance  
= Work done

Distance/time =  
velocity

The various forces acting on the fluid

Element axis

Force ( $P_x dA$ ) acting at section ① - ①

- 1) The pressure force  $(P + dp) dA$  acting at section ② - ②

- 3) The weight component  $w \cos\theta$  or  $\rho g dA d$  acting at section ③ - ③

Let  $\theta$  is the angle b/w the direction of flow & the line of action of the weight of element.

A/c to Newton's second law of motion

we have,

$$F = ma$$

Selecting substituting the values of 'F' in Newton's law, we get.

$$(P_x dA) - [(P + dp) dA] - (\rho g dA ds \cos\theta) = ma$$

$$P dA - P dA - dp dA - \rho g dA ds \cos\theta = S dA ds \cdot a$$

$$dp dA = -g dA ds \frac{dv}{dt} - \rho g dA ds \cos\theta$$

$$\therefore \frac{dp}{\rho g dA} = -\frac{dv}{ds} \frac{ds}{dt} - g \cos\theta \quad \left(\because a = \frac{dv}{dt}\right)$$

$$\frac{dp}{\rho g dA} = -\frac{dv}{ds} - g \cos\theta$$

$$\frac{dp}{\rho g dA} = -\frac{ds}{dt} \frac{dv}{ds} - g \cos\theta$$

$$V \cdot \frac{dv}{ds} + g \cos\theta + \frac{dp}{\rho ds} = 0 \quad (5)$$

$$\therefore \frac{ds}{dt} = V$$

From the fig.,  $\cos\theta = \frac{dz}{ds}$

$$V \cdot \frac{dv}{ds} + g \frac{dz}{ds} + \frac{dp}{\rho ds} = 0$$

$x$  is on b.s.d

$$V \cdot \frac{dv}{ds} + g \frac{dz}{ds} + \frac{dp}{\rho ds} = 0 \rightarrow (A)$$

This eqn is known as Euler's eqn

Bernoulli's Equation from Euler's eqn

L.H.T Euler's eqn ;  $V \frac{dv}{ds} + g \frac{dz}{ds} + \frac{dp}{\rho s g} = 0$   
 $\downarrow$  by  $\frac{1}{g}$  on L.H.T

$$V \frac{dv}{g} + dz + \frac{dp}{\rho g} = 0$$

Integrating above eqn

$$\int V \frac{dv}{g} + \int dz + \frac{1}{\rho g} \int dp = \text{constant}$$

$$\frac{V^2}{2g} + z + \frac{p}{\rho g} = \text{constant} \rightarrow (B)$$

This eqn is known as Bernoulli's eqn or it represents the total energy per unit weight of the fluid.

where:  $\frac{P}{\rho g}$  → Pressure energy per unit weight  
or pressure head of fluid.

$\frac{V^2}{2g}$  → kinetic energy per unit weight or kinetic head.

$z$  → potential energy per unit weight or potential head

Explain by eqn (B)

i.e., 
$$\boxed{\frac{V^2}{2} + zg + \frac{P}{\rho g} = \text{constant}} \rightarrow \textcircled{C} \text{ this Eqn}$$
  
represents total weight per unit mass.

Defn.

(6)

Derivative of Bernoulli's eqn from energy principle:-

Statement: Bernoulli's theorem based on the principle of conservation of energy states that, ' In a steady continuous incompressible non-viscous fluid, the sum of the potential head (datum head), velocity head & pressure head is same at all points " or in other words " the total energy remains constant for a ideal steady incompressible fluid flowing continuously". or for a perfect incompressible fluid flowing continuously the sum of the total energy at any point is the same".

Mathematically, we have

$$\frac{V^2}{2g} + \frac{P}{\rho g} + z = \text{constant}$$

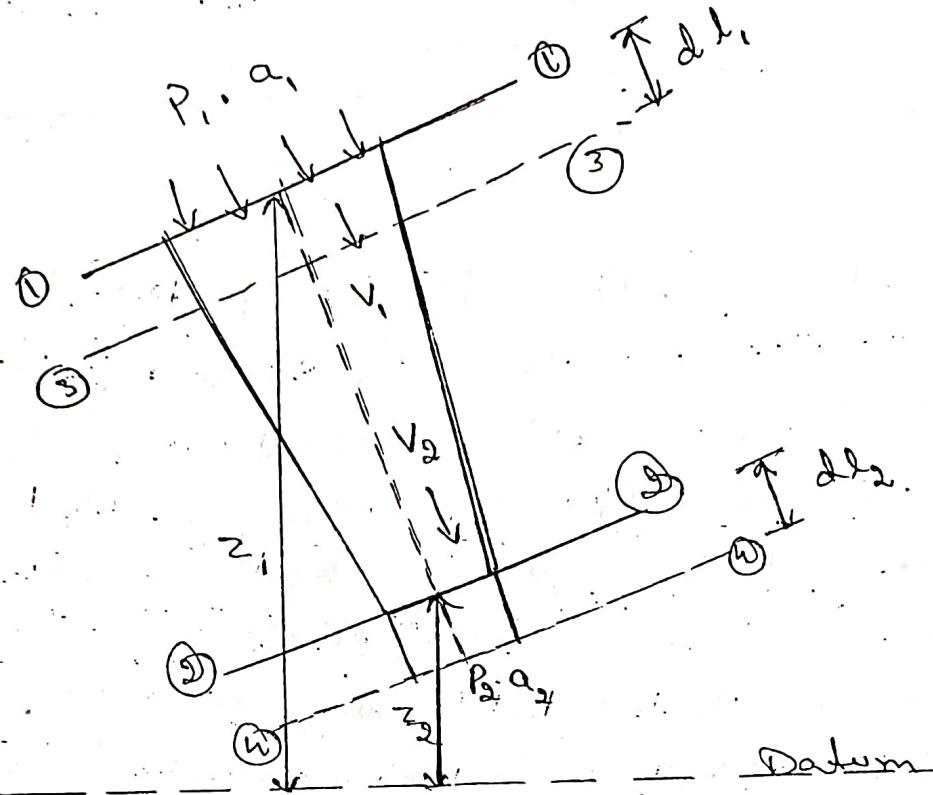
(or)

$$\boxed{\frac{V_1^2}{2g} + z_1 + \frac{P_1}{\rho g} = \frac{V_2^2}{2g} + z_2 + \frac{P_2}{\rho g}}$$

Assumptions:-

- 1) Fluid is ideal
- 2) Fluid is continuous
- 3) Fluid is steady
- 4) Fluid is incompressible
- 5) Fluid is irrotational

Proof!



Consider a liquid which is incompressible, frictionless with steady condition flowing continuously through a pipe as shown in the fig. The fluid filled in the pipe be under pressure.

Let,  $z_1, P_1, V_1, A_1$  represents datum height, pressure, velocity &  $A_1$  area at section ①-①. Similarly  $z_2, P_2, V_2 \& A_2$  represents corresponding values at section ②-②.

Let the quantity of liquid b/w the section ①-① & ②-② moves to ①-① & ④-④ by a small distance  $dl_1$  &  $dl_2$  as shown in fig. So that the movement of the liquid b/w ①-① & ④-④ is equivalent to the movement of liquid b/w ④-④ & ⑤-⑤.

Let  $w$  be the total weight of the fluid &  $\omega$  specific weight of the fluid.

$$\therefore \text{Weight of the fluid b/w } \left. \begin{array}{l} \textcircled{1}-\textcircled{2} \& \textcircled{3}-\textcircled{4} \end{array} \right\} = \text{Sp. wt} \times \text{Volume}$$

$$\text{i.e., } w = \omega \times a_1 d l_1$$

$$\text{Similarly wt of the fluid b/w } \left. \begin{array}{l} \textcircled{2}-\textcircled{3} \& \textcircled{4}-\textcircled{5} \end{array} \right\} (w) = \omega a_2 d l_2$$

Since the flow is continuous,

$$w = \omega a_1 d l_1 = \omega a_2 d l_2$$

$$(or) \frac{w}{\omega} = a_1 d l_1 = a_2 d l_2 \rightarrow \textcircled{1}$$

The workdone by the pressure at the section  $\textcircled{1}-\textcircled{2}$  in moving the liquid to the section  $\textcircled{2}-\textcircled{3}$  is  
= Force  $\times$  distance

$$= P_1 a_1 \times d l_1 \quad (\because \text{Force} = P a)$$

likewise, the workdone by the pressure at the section  $\textcircled{2}-\textcircled{3}$  in moving the liquid to the section  $\textcircled{3}-\textcircled{4}$  is

$$= P_2 a_2 \times d l_2$$

$$\therefore \text{Total Workdone} = P_1 a_1 d l_1 - P_2 a_2 d l_2 \rightarrow \textcircled{2}$$

But, from eqn  $\textcircled{1}$  we have  $\frac{w}{\omega} = a_1 d l_1 = a_2 d l_2$

$\therefore$  Eqn  $\textcircled{2}$  becomes i.e.

$$\begin{aligned} \text{Total Workdone} &= P_1 \frac{w}{\omega} - P_2 \frac{w}{\omega} \\ &= (P_1 - P_2) \frac{w}{\omega} \rightarrow \textcircled{3} \end{aligned}$$

Since the fluid has been moved from ① to ② to ③ - ④ & ⑤ - ⑥ to ⑦ - ⑧ there will be loss of datum energy which will be given by  $\Delta z$ .

$$\text{Loss of datum energy (DE)} = W [z_1 - z_2]$$

Then, the gain of ~~kinetic~~ kinetic energy is given by,

$$\text{gain of K.E} = W \left[ \frac{v_2^2}{2g} - \frac{v_1^2}{2g} \right]$$

$\therefore a = \alpha, v_1 = \alpha_1$   
where  $a_2$  is less  
hence  $v_2$  is more.

For the above system, we have

$$\text{Total workdone + loss of DE} = \text{gain of K.E}$$

$$\frac{W}{\omega} (P_1 - P_2) + W(z_1 - z_2) = W \left[ \frac{v_2^2}{2g} - \frac{v_1^2}{2g} \right]$$

$$\frac{P_1}{\omega} - \frac{P_2}{\omega} + z_1 - z_2 = \frac{v_2^2}{2g} - \frac{v_1^2}{2g}$$

(or)

$$\boxed{\frac{P_1}{\omega} + z_1 + \frac{v_1^2}{2g} = \frac{P_2}{\omega} + z_2 + \frac{v_2^2}{2g}} \rightarrow \textcircled{A}$$

From this eqn it is very clear that the sum of pressure energy, datum energy & kinetic energy remains constant for a continuous flowing incompressible fluid

$$\boxed{\frac{v^2}{2g} + z + \frac{P}{\omega} = \text{constant}}$$

## Limits of Bernoulli's Principle

- 1) It has been taken into account that the velocity is constant through the pipe, but in actual practice it is not true since the velocity is maximum at the centre & it slowly decreases at the walls due to friction. Hence average velocity must be taken into account.
- 2) Flow is not steady in actual practice.
- 3) All the external forces must be taken into account.
- 4) Liquid is not always incompressible.
- 5) The concept of ideal fluid does not hold good in real practice.
- 6) When the fluid is flowing along a curved path the energy due to centripetal force must be taken into account.
- 7) It has been assumed that there is loss of energy during the flow. But in case of turbulent flow some amount of energy is converted into heat energy & in case of viscous flow some amount of energy is lost due to shear force. Hence these losses must be taken in account in real practice.

## Modified Bernoulli's equation or Bernoulli's eqn for real fluids

By deriving Bernoulli's eqn it was assumed that the fluid is ideal & non-viscous or frictionless. However, in actual practice the fluids are real having viscosity & hence during the flow of liquids it offers resistance. Due to this resistance there exists certain losses which are not taken into account during the derivation of Bernoulli's eqn. Hence, the Bernoulli's eqn. for real fluids is given by the correction.

$$\frac{P_1}{\rho} + z_1 + \frac{V_1^2}{2g} = \frac{P_2}{\rho} + z_2 + \frac{V_2^2}{2g} + h_L$$

where,  $h_L \rightarrow$  head loss or energy loss.

### Applications of Bernoulli's eqn

Bernoulli's eqn is applied for all problems of incompressible fluid flows where energy is involved. It is used for flow measuring devices which are based on the principle that as the flow accelerates (velocity increases) corresponding the pressure decreases. The drop or decrease of pressure can be measured conveniently & correlated to the discharge. The various flow measuring devices based on Bernoulli's eqn are:

- 1) venturimeter, 2) orifice meter, 3) Pitot tube.

(a)

Water is flowing problems through a pipe of 5 cm dia. under a pressure of 29.43 N/cm<sup>2</sup> (gauge) & with mean velocity of 2.0 m/sec. Find the total head or total energy per unit weight of the water at a C/S, which is 5 m above the datum line.

Soln:- Given

$$\text{Dia. of pipe} = 5 \text{ cm} = 0.05 \text{ m}$$

$$\text{Pressure } (P) = 29.43 \text{ N/cm}^2 = 29.43 \times 10^4 \text{ N/m}^2$$

$$\text{Velocity } (V) = 2.0 \text{ m/sec}$$

$$z = 5 \text{ m}$$

Total head = pressure head + kinetic head + elevation head

$$\therefore \text{Pressure head} = \frac{P}{\rho g} = \frac{29.43 \times 10^4}{1000 \times 9.81} = 30 \text{ m}$$

$$\text{Kinetic head} = \frac{V^2}{2g} = \frac{2 \times 2}{2 \times 9.81} = 0.204 \text{ m}$$

$$\therefore \text{Total head} = \frac{P}{\rho g} + \frac{V^2}{2g} + z = 30 + 0.204 + 5 \\ = 35.204 \text{ m}$$

(b) A pipe, through which water is flowing, is having diameters, 20 cm & 10 cm at the C/S (1) & (2) respectively. The velocity of water at section (1) is given 4.0 m/sec. Find the velocity head at section (1) & (2) & also rate of discharge.

Sol'n) Given:

$$D_1 = 20 \text{ cm} = 0.2 \text{ m}$$

$$A_1 = \frac{\pi D_1^2}{4} = \frac{\pi (0.2)^2}{4} = 0.0314 \text{ m}^2$$

$$V_1 = 4.0 \text{ m/sec}$$

$$D_2 = 0.1 \text{ m}$$

$$A_2 = \frac{\pi (D_2)^2}{4} = 0.00785 \text{ m}^2$$

(i) Velocity head at section ①

$$= \frac{V_1^2}{2g} = \frac{4 \times 4}{2 \times 9.81} = 0.815 \text{ m}$$

(ii) velocity head at section ② =  $\frac{V_2^2}{2g}$

To find  $V_2$ , apply continuity eqn at ① & ②

$$\therefore A_1 V_1 = A_2 V_2$$

$$\text{Cont. } V_2 = \frac{A_1 V_1}{A_2} = \frac{0.0314 \times 4}{0.00785}$$

$$= \frac{0.0314 \times 4}{0.00785} = 1.6 \text{ m/sec}$$

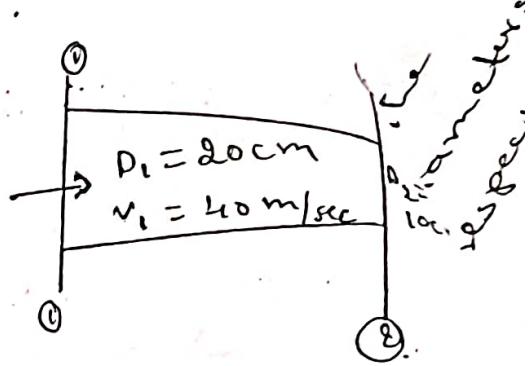
velocity head at section ② =  $\frac{V_2^2}{2g}$

$$= \frac{1.6 \times 1.6}{2 \times 9.81} = 83.047 \text{ m}$$

(iii) Rate of discharge =  $A_1 V_1$  or  $A_2 V_2$

$$= 0.0314 \times 4 = 0.1256 \text{ m}^3/\text{sec}$$

$$= 125.6 \text{ litres/sec}$$



The water is flowing through a pipe having diameters 20cm & 10cm at section (1) & (2) respectively. The rate of flow through pipe is 35 litres/sec. The section - (1) is 6m above datum & section - (2) is 4m above datum. If the pressure at section (1) is 39.24 N/cm<sup>2</sup>, find the intensity of pressure at section - (2).

Soln:- Given:

At section - (1)

$$D_1 = 20\text{ cm} = 0.2\text{ m}$$

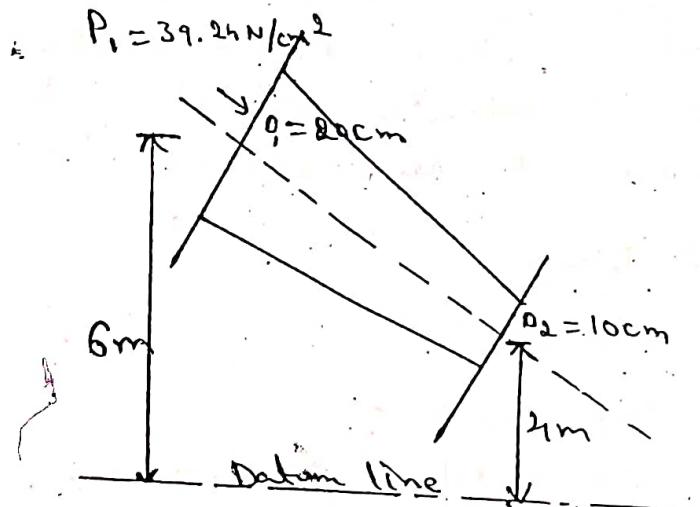
$$A_1 = \frac{\pi}{4}(D_1)^2 = \frac{\pi}{4}(0.2)^2$$

$$A_1 = 0.0314\text{ m}^2$$

$$P_1 = 39.24 \text{ N/cm}^2$$

$$= 39.24 \times 10^4 \text{ N/m}^2$$

$$z_1 = 6.0 \text{ m}$$



∴ Rate of flow,  $Q = 35 \text{ lit/sec}$

At section - (2)

$$D_2 = 10\text{ cm} = 0.1\text{ m}$$

$$A_2 = \frac{\pi}{4}(D_2)^2 = \frac{\pi}{4} \times (0.1)^2$$

$$A_2 = 0.00785 \text{ m}^2$$

$$z_2 = 4 \text{ m}$$

$$P_2 = ?$$

$$Q = A_1 V_1 = A_2 V_2$$

$$V_1 = \frac{Q}{A_1} \quad \& \quad V_2 = \frac{Q}{A_2}$$

$$\therefore V_1 = \frac{35 \times 10^{-3}}{0.0314} = 1.114 \text{ m/sec}$$

$$V_2 = \frac{35 \times 10^{-3}}{0.00785} = 4.456 \text{ m/sec}$$

Applying Bernoulli's eqn at section (1) & (2) we get

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + z_2$$

$$\frac{39.24 \times 10^4}{1000 \times 9.81} + \frac{(1.114)^2}{2 \times 9.81} + 6 = \frac{P_2}{1000 \times 9.81} + \frac{(4.456)^2}{2 \times 9.81} +$$

$$P_2 = 40.27 \text{ N/cm}^2$$

Q) Water is flowing through a pipe having diameter 300mm & 200mm at the bottom & upper end respectively. The intensity of pressure at the bottom end is 24.525 N/cm<sup>2</sup> & the pressure at the upper end is 9.81 N/cm<sup>2</sup>. Determine the difference in datum head if the rate of flow through pipe is 40 lit/sec.

Solu:- Given

At section - ①

$$D_1 = 300 \text{ mm} = 0.3 \text{ m}$$

$$P_1 = 24.525 \text{ N/cm}^2 = 24.525 \times 10^4 \text{ N/m}^2$$

At section - ②

$$D_2 = 200 \text{ mm} = 0.2 \text{ m}$$

$$P_2 = 9.81 \text{ N/cm}^2 = 9.81 \times 10^4 \text{ N/m}^2$$

$$Q = 40 \text{ lit/sec} = 40 \times 10^{-3} \text{ m}^3/\text{sec}$$

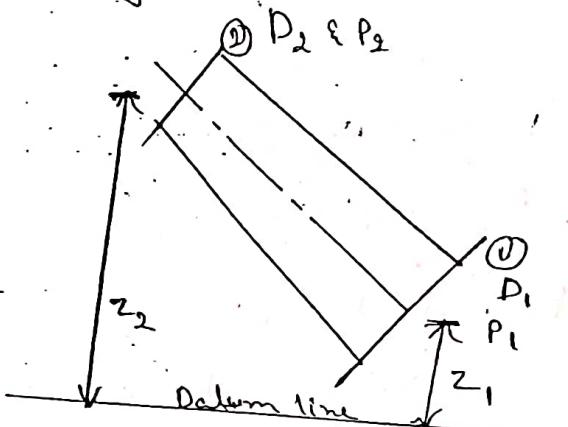
$$\text{Now; } A_1 V_1 = A_2 V_2 = \text{rate of flow} = 0.04 \text{ m}^3/\text{sec}$$

$$V_1 = \frac{Q}{A_1} = \frac{0.04}{\frac{\pi}{4} \times D_1^2} = \frac{0.04}{\frac{\pi}{4} \times (0.3)^2} = 0.5658 \text{ m/sec}$$

$$V_2 = \frac{Q}{A_2} = \frac{0.04}{\frac{\pi}{4} \times D_2^2} = \frac{0.04}{\frac{\pi}{4} \times (0.2)^2} = 1.27 \text{ m/sec}$$

Apply Bernoulli's eqn at section - ① & ②

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + z_2$$



$$\frac{24.525 \times 10^3}{1000 \times 9.81} + \frac{(0.5658)^2}{2 \times 9.81} + z_1 = \frac{9.81 \times 10^3}{1000 \times 9.81} + \frac{(1.274)^2}{2 \times 9.81} + z_2$$

$$\therefore (z_2 - z_1) = 25 + 0.0163 - 10 - 0.0827$$

$$z_2 - z_1 = 14.933 \text{ m}$$

5) A pipe of dia 400 mm carries water at a velocity of 25 m/sec. The pressures at the points A & B are given as 29.43 N/cm<sup>2</sup> & 22.563 N/cm<sup>2</sup> respectively while the datum head at 'A' & 'B' are 28m & 30m. Find the loss of head b/w A & B.

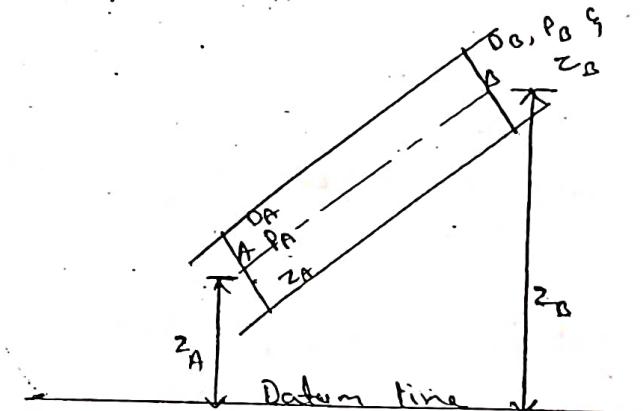
Soln: Given:-

$$\text{Dia of pipe (D)} = 400 \text{ mm} = 0.4 \text{ m}$$

$$\text{velocity (V)} = 25 \text{ m/sec}$$

At point (A);

$$P_A = 29.43 \text{ N/cm}^2 \\ = 29.43 \times 10^4 \text{ N/m}^2$$



$$z_A = 28 \text{ m}$$

$$V_A = V = 25 \text{ m/sec}$$

$$\therefore \text{Total energy at A}, E_A = \frac{P_A}{\rho g} + \frac{V_A^2}{2g} + z_A$$

$$= \frac{29.43 \times 10^4}{1000 \times 9.81} + \frac{(25)^2}{2 \times 9.81} + 28$$

$$= 89.855 \text{ m}$$

At point (B);

$$P_B = 22.563 \text{ N/cm}^2$$

$$z_B = 30 \text{ m}$$

$$V_B = V = 25 \text{ m/sec}$$

$$\therefore \text{Total energy at B}, (E_B) = \frac{P_B}{\rho g} + \frac{V_B^2}{2g} + z_B$$

$$= \frac{22.563 \times 10^4}{1000 \times 9.81} + \frac{(25)^2}{2 \times 9.81} + 30$$

$$E_B = 84.855 \text{ m}$$

$$\therefore \text{Loss of energy} = E_A - E_B = 89.855 - 84.855 \\ = 5.0 \text{ m}$$

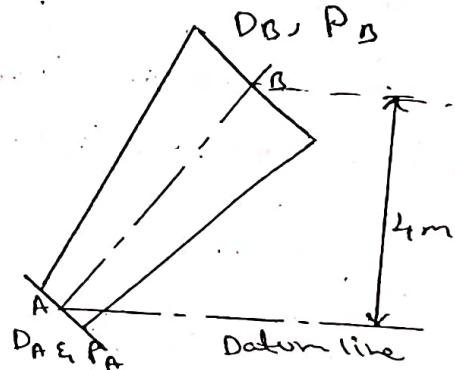
6) A pipeline carrying oil of specific gravity 0.8 changes in diameter from 200mm diameter at a position 'A' to 500mm diameter at a position 'B' which is 4m at a higher level. If the pressures at 'A' & 'B' are 9.81 N/cm<sup>2</sup> & 5.886 N/cm<sup>2</sup> respectively & the discharge is 200 litre/sec determine the loss of head & direction of flow

Soln: Given

$$\text{Discharge (Q)} = 200 \text{ lit/sec} \\ = 0.2 \text{ m}^3/\text{sec}$$

$$\text{Sp. gr of oil} = 0.87$$

$$\therefore \rho \text{ of oil} = 0.87 \times 1000 \\ = 870 \text{ kg/m}^3$$



At section (A):

$$D_A = 200 \text{ mm} = 0.2 \text{ m}$$

$$A_A = \frac{\pi}{4} (D_A)^2 = \frac{\pi}{4} (0.2)^2$$

$$A_A = 0.0314 \text{ m}^2$$

$$P_A = 9.81 \text{ N/cm}^2$$

$$= 9.81 \text{ kN/m}^2$$

$$P_A = 9.81 \times 10^4 \text{ N/m}^2$$

$$z_A = 0$$

At section (B):

$$D_B = 500 \text{ mm} = 0.5 \text{ m}$$

$$A_B = \frac{\pi}{4} (D_B)^2 = \frac{\pi}{4} (0.5)^2 = 0.1963 \text{ m}^2$$

$$P_B = 5.886 \text{ N/cm}^2$$

$$= 5.886 \times 10^4 \text{ N/m}^2$$

$$z_B = 4 \text{ m}$$

$$\therefore V_A = \frac{Q}{A_0} = \frac{0.2}{0.0314} = 6.369 \text{ m/sec}$$

(12)

$$\therefore V_B = \frac{Q}{A_0} = \frac{0.2}{0.1963} = 1.018 \text{ m/sec}$$

$$\begin{aligned}\text{Total energy (A)} &= E_A = \frac{P_A}{\rho g} + \frac{V_A^2}{2g} + z_A \\ &= \frac{9.81 \times 10^4}{0.87 \times 1000 \times 9.81} + \frac{(6.369)^2}{2 \times 9.81} + 0 \\ &= \underline{\underline{13.56 \text{ m}}}\end{aligned}$$

$$\begin{aligned}\text{Total energy (B)} &= E_B = \frac{P_B}{\rho g} + \frac{V_B^2}{2g} + z_B \\ &= \frac{5.886 \times 10^4}{870 \times 9.81} + \frac{(1.018)^2}{2 \times 9.81} + 4 \\ &= \underline{\underline{10.959 \text{ m}}}\end{aligned}$$

(i) Direction of flow: As  $E_A$  is more than  $E_B$   
hence flow is taking place from A to B.

(ii) Loss of head ( $h_L$ ) =  $E_A - E_B$

$$= 13.56 - 10.95 = 2.61 \text{ m}$$

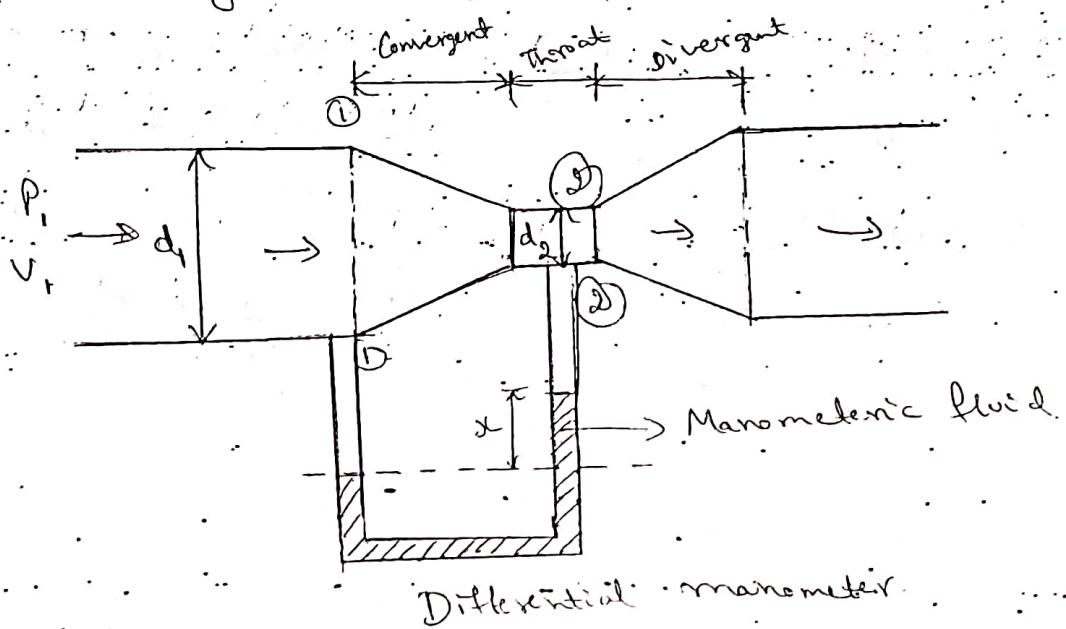
## Venturi meter:-

Venturi meter is a device works on the principle of Bernoulli's equation & used for the measurement of discharge through a pipe.

The Bernoulli's principle was first demonstrated by G.B. Venturi, an Italian physicist in 1797. But the principle was first applied to the instrument was invented by an American engineer CLEMENS HERSWEL in 1887.

Venturi meter is convenient for large size discharges. Efficiency is high & pressure recovery is greater. But its initial cost is high. It consists of 3 parts namely;

- a) Convergent
- b) Throat
- c) Divergent



(13)

Consider a venturi meter as shown in fig. Let  
 $d_1$  be the dia at the inlet,  $P_1 \rightarrow$  pressure at ① - ①  
 $V_1 \rightarrow$  velocity at ① - ①.  
 $a_1 \rightarrow$  cross area at ① - ①.

Similarly  $d_2$ ,  $P_2$ ,  $V_2$ ,  $a_2$  corresponding values at section ② - ②. As the fluid flows through the convergent position the velocity increases corresponding pressure decreases. Applying the Bernoulli's eqn. b/w the section ① - ① & ② - ② we have,

$$\frac{P_1}{\rho g} + z_1 + \frac{V_1^2}{2g} = \frac{P_2}{\rho g} + z_2 + \frac{V_2^2}{2g}$$

Taking the centre line of the venturi meter as datum.

then,  $z_1 = z_2$  (pipe is horizontal)

$$\therefore \frac{P_1}{\rho g} + \frac{V_1^2}{2g} = \frac{P_2}{\rho g} + \frac{V_2^2}{2g}$$

$$(\text{or}) \quad \frac{P_1}{\rho g} - \frac{P_2}{\rho g} = \frac{V_2^2}{2g} - \frac{V_1^2}{2g}$$

$$(\text{or}) \quad h = \frac{V_2^2 - V_1^2}{2g}$$

$$V_2^2 - V_1^2 = 2gh \rightarrow ①$$

W.L.C.T by continuity eqn.,  $Q = a_1 V_1 = a_2 V_2$

$$V_1 = \frac{a_2 V_2}{a_1}$$

Sub. in eqn ①, we get;

$$V_2^2 - \frac{a_2^2 V_2^2}{a_1^2} = 2gh$$

$$V_2^2 \left[ 1 - \frac{a_2^2}{a_1^2} \right] = 2gh$$

$$(or) \quad V_2^2 \left[ \frac{a_1^2 - a_2^2}{a_1^2} \right] = 2gh$$

Also, W.K.T.  $\frac{Q}{a_2} = V_2$

$$\therefore \frac{Q^2}{a_2^2} = \frac{a_1^2 \times 2gh}{a_1^2 - a_2^2}$$

$$\therefore Q^2 = \frac{a_1^2 \times a_2^2 \times 2gh}{a_1^2 - a_2^2}$$

$$(or) \quad Q = \frac{a_1 a_2 \sqrt{2gh}}{\sqrt{a_1^2 - a_2^2}}$$

Note:- 1) The above eqn gives the theoretical discharge through the venturiometer. But in actual practice the actual discharge is less than the theoretical discharge.

W.K.T. Actual discharge is given by,

$$C_d = \frac{Q_{act}}{Q_{theo}}$$

( $C_d$  = Co-efficient of venturiometer & its value is less than 1)

$$\therefore Q_{act} = C_d \times Q_{theo}$$

(15)

$$Q_{act} = C_d \times \frac{a_1 a_2 \sqrt{2gh}}{\sqrt{a_1^2 - a_2^2}}$$

2) The value of  $h$  has to be determined by using a differential manometer.

Case(1):- Let  $S_m \rightarrow$  sp. gravity of manometric liquid (heavy fluid)

$S \rightarrow$  sp. gravity of metering fluid  
 $x \rightarrow$  manometer reading.

The pressure head is given by.

$$h = x \left[ \frac{S_m}{S} - 1 \right]$$

Case(2):- If the differential manometer contains fluid lighter than the fluid flowing in the pipe. Then the differential head is given by

$$h = x \left[ 1 - \frac{S_m}{S} \right]$$

Problems

1) A horizontal venturi meter with inlet & throat diameter 30cm & 15cm respectively is used to measure the flow of water. The reading of differential manometer connected to the inlet & the throat is 20cm of mercury. Determine the rate of flow. Take  $C_d = 0.98$ .

Soln:- Given,  $d_1 = 30\text{cm} = 0.3\text{m}$

$$d_2 = 15\text{cm} = 0.15\text{m}$$

$$x = 20\text{cm}$$

$$C_d = 0.98$$

$$\therefore \text{Area of inlet}; a_1 = \frac{\pi d_1^2}{4} = 0.07\text{ m}^2$$

$$\text{Area of throat}; a_2 = \frac{\pi d_2^2}{4} = \frac{\pi \times (0.15)^2}{4} = 0.0176\text{ m}^2$$

The pressure head is given by:

$$h = x \left[ \frac{S_m}{s} - 1 \right] = 0.2 \left[ \frac{13.6}{1} - 1 \right] = 2.52 \text{ m of H}_2\text{O}$$

$$\therefore \text{Discharge}, Q_{act} = \frac{C_d \times a_1 a_2 \sqrt{2gh}}{\sqrt{a_1^2 - a_2^2}}$$

$$= 0.98 \times 0.07 \times 0.0176 \times \sqrt{2 \times 9.81 \times 2.52}$$

$$\sqrt{0.07^2 - 0.0176^2}$$

$$Q_{act} = 0.125 \text{ m}^3/\text{sec}$$

(15)

An oil of sp. gravity 0.8 is flowing through a venturimeter having inlet diameter 20cm & throat diameter 10cm. The oil-mercury differential manometer shows a reading of 25cm. Calculate the discharge of oil through the horizontal venturimeter. Take  $C_d = 0.98$ .

Soln:- Given:  $S_o = 0.8$ ,  $S_m = 13.6$ ,  $d_1 = 20\text{cm} = 0.2\text{m}$   
 $d_2 = 10\text{cm} = 0.1\text{m}$ ,  $\Delta h = 25\text{cm} = 0.25\text{m}$   
 $C_d = 0.98$ ;  $Q = ?$

$$h = \Delta h \left[ \frac{S_m}{S_o} - 1 \right] = 0.25 \left[ \frac{13.6}{0.8} - 1 \right] = 4\text{m}$$

$$a_1 = \frac{\pi}{4} d_1^2 = \frac{\pi}{4} (0.2)^2 = 0.03\text{ m}^2$$

$$a_2 = \frac{\pi}{4} d_2^2 = \frac{\pi}{4} (0.1)^2 = 0.00785\text{ m}^2$$

$$\therefore Q_{act} = C_d \times \frac{a_1 a_2 \sqrt{2gh}}{\sqrt{a_1^2 - a_2^2}} = \frac{0.98 \times 0.03 \times 0.00785 \times \sqrt{2 \times 9.8 \times 4}}{\sqrt{0.03^2 - 0.00785^2}}$$

$$(Q = 0.0706\text{ m}^3/\text{sec} = 70.6\text{ lit/sec})$$

- 3) A horizontal Venturimeter with inlet dia 20cm & throat dia 10cm is used to measure the flow of oil of sp. gravity 0.8. The discharge of oil through venturimeter is 60 lit/sec. Find the reading of the oil-mercury differential manometer. Take  $C_d = 0.98$ .

$\therefore \text{Head Lost } (h_L) = 4\% \text{ of } h$

$$= \frac{4}{100} \times 19.032 = 0.761 \text{ m}$$

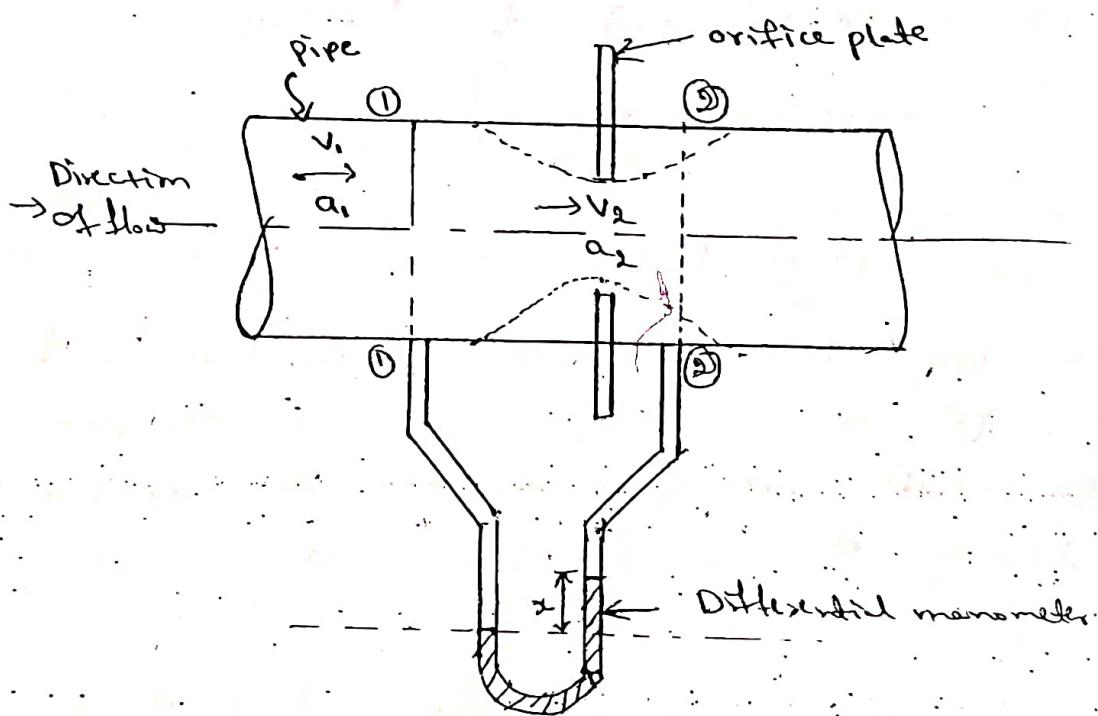
$$\therefore C_d = \sqrt{\frac{h - h_L}{h}} = \sqrt{\frac{19.032 - 0.761}{19.032}} = 0.979$$

$$\therefore Q = \frac{C_d \times a_1 a_2 \times \sqrt{2gh}}{\sqrt{a_1^2 - a_2^2}} = \frac{0.98 \times 0.0706 \times 0.00785 \times}{\sqrt{2 \times 9.81 \times 19.03}} \\ \sqrt{0.0706^2 - 0.00785^2}$$

$$Q = 0.1495 \text{ m}^3/\text{sec} \approx 0.15 \text{ liter/sec} = 150 \text{ liter/sec}$$

## Orifice meter:

Orifice meter works on the principle of Bernoulli's law & used for the measurement of discharge through the pipe similar to that of venturiometer. It consists of a flat circular plate which has a circular sharp edged hole called orifice, which is concentric with the pipe. The orifice diameter is kept generally 0.5 time the diameter of the pipe, though it may vary from 0.4 to 0.8 times the pipe diameter.



At the orifice the cross area of flow decreases & velocity increases which in turn reduces the pressure to that of the inlet. However, to Bernoulli's law the total energy remains constant. Hence according to Bernoulli's law the discharge through the orifice meter can be obtained similar to that of venturiometer.

$$\therefore Q_{\text{theo}} = \frac{a_1 a_2 \sqrt{2gh}}{\sqrt{a_1^2 - a_2^2}}$$

But, the actual discharge is given by,

$$Q_{\text{act}} = Cd * Q_{\text{theo}}$$

$$\therefore Q_{\text{act}} = \frac{Cd * a_1 a_2 \sqrt{2gh}}{\sqrt{a_1^2 - a_2^2}}$$

Where,  $a_1 \rightarrow$  Clean area of the pipe.

$a_2 \rightarrow$  clean area of the orifice.

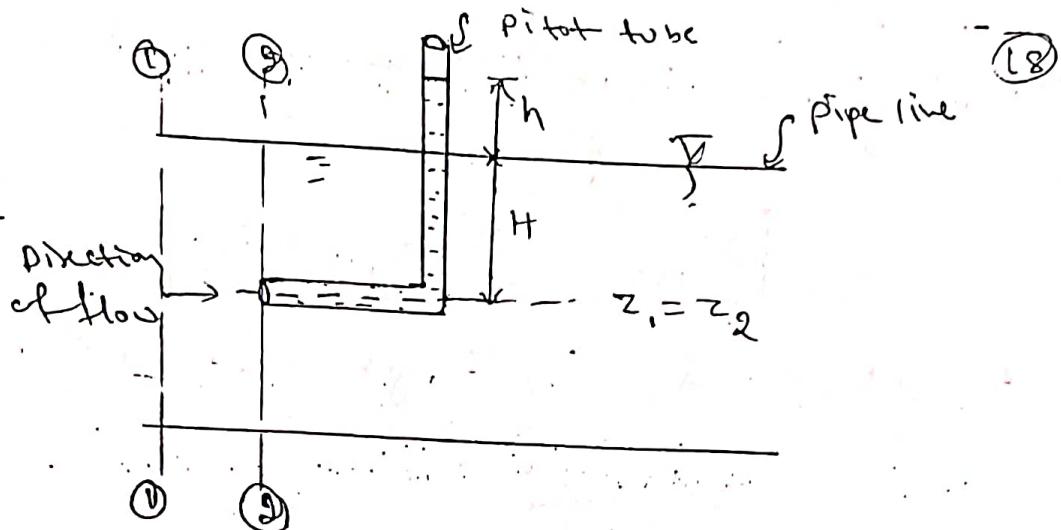
$Cd \rightarrow$  Co-efficient of discharge

[varies 0.61 - 0.66]

### Pitot tube:-

A pitot tube is a simple glass tube bent through  $90^\circ$  or L-shape, works on the principle of Bernoulli's eqn & used for the measurement of velocity of flow in a continuous flowing fluid.

A pitot tube having the pointed & short length is kept usually facing the direction of flow as shown in fig.



As the fluid enters the pitot tube the velocity get reduced to zero & the pressure at that point is termed as stagnation pressure. Applying Bernoulli's eqn b/w the stagnation point & the upstream of the flowing liquid.

$$\frac{P_1}{\rho g} + z_1 + \frac{V_1^2}{2g} = \frac{P_2}{\rho g} + z_2 + \frac{V_2^2}{2g}$$

Taking the centre line of the pitot tube as the datum we have,  $z_1 = z_2$  & at stagnation point,  $V_2 = 0$ .

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} = \frac{P_2}{\rho g}$$

$$\frac{V_1^2}{2g} = \frac{P_1 - P_2}{\rho g}$$

$$\text{i.e. } \frac{V_1^2}{2g} = h$$

$$\therefore V_1 = \sqrt{2gh} \quad \text{or} \quad V = \sqrt{2gh}$$

The velocity so obtained is known as theoretical velocity. However, the actual velocity is given by  $V_{act.} = V_{theo.} \times C_V$

where,  $C_v \rightarrow$  coefficient of velocity of  
pitot tube

$$\therefore V_{\text{act}} = C_v \times \sqrt{2gh}$$

The value of  $C_v$  ranges b/w 0.95 to 0.98

### Problem

1) In a vertical pipe conveying oil of sp.gr. 0.8, two pressure gauges have been installed at A & B where the diameters are 16cm & 8cm respectively. A is 2m above B. The pressure gauge readings have shown that the pressure at B is greater than at A by 0.981 N/cm<sup>2</sup>. Neglecting all losses, calculate the flow rate. If the gauges at A & B are replaced by tubes filled with the same liquid & connected to a U-tube containing mercury. Calculate the difference of level of mercury in the 2 limbs of the tube.

Sol:- Given:  $\rho_o = 0.8$

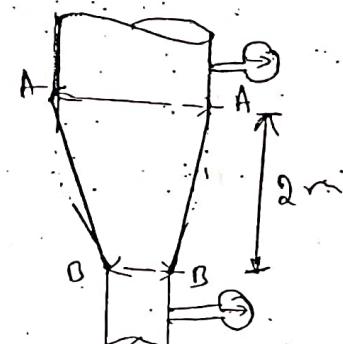
$$d_A = 16 \text{ cm} = 0.16 \text{ m}$$

$$d_B = 8 \text{ cm} = 0.08 \text{ m}$$

$$z_A = 2 \text{ m}$$

$$\begin{aligned} \text{Difference of Pressure, } P_B - P_A &= 0.981 \text{ N/cm}^2 \\ &= 0.981 \times 10^4 \text{ N/m}^2 \end{aligned}$$

$$\therefore \text{Area at A. } (A_A) = \frac{\pi d_A^2}{4} = \frac{\pi (0.16)^2}{4} = 0.02 \text{ m}^2$$



$$a_0 = \frac{\pi d_0^2}{4} = \frac{\pi \times (0.08)^2}{4} = 0.00502 \text{ m}^2 \quad (19)$$

∴ Difference of Pressure head,  $\frac{P_0 - P_A}{\rho g} = \frac{0.981 \times 10^4}{0.8 \times 1000 \times 9.81}$

$$= 1.25$$

Taking datum at '0', & applying Bernoulli's eqn, we have

$$\therefore \frac{P_A}{\rho g} + z_A + \frac{V_A^2}{2g} = \frac{P_0}{\rho g} + z_0 + \frac{V_0^2}{2g} \quad (20)$$

$$\frac{P_B}{\rho g} - \frac{P_A}{\rho g} = +z_A - z_B + \frac{V_A^2}{2g} - \frac{V_B^2}{2g}$$

$$\therefore 1.25 = 0 - 0 + \frac{V_A^2}{2g} - \frac{V_B^2}{2g}$$

$$\frac{V_A^2}{2g} - \frac{V_B^2}{2g} = 0.75$$

Applying continuity eqn, ie,  $Q = a_A V_A = a_0 V_0$

$$\therefore V_0 = \frac{a_A V_A}{a_0}$$

Sub  $\frac{a_A V_A^2}{a_0^2 g} = \frac{V_A^2}{2g} = 0.75$

i.e,  $\frac{(0.02)^2 V_A^2}{(0.00502)^2 (2 \times 9.81)} = \frac{V_A^2}{(2 \times 9.81)} = 0.75$

$$0.809 V_A^2 - 0.0509 V_A^2 = 0.75$$

$$V_A^2 = \frac{0.75}{0.758}$$

$$V_A^2 = 0.989$$

$$\therefore V_A = 0.995 \text{ m/sec}$$

$$\therefore \text{Rate of flow, } Q = c_A V_A = 0.02 \times 0.995$$

$$Q = 0.0199 \text{ m}^3/\text{sec}$$

(ii) Difference of level of mercury in the U-tube

$$h = x \left[ \frac{S_m}{S_o} - 1 \right]$$

$$\text{where, } h = \left[ \frac{P_A}{\omega} + z_A \right] - \left[ \frac{P_o}{\omega} + z_o \right]$$

$$h = \frac{P_A}{\omega} - \frac{P_o}{\omega} + z_A - z_o$$

$$h = -1.25 + 2 = 0.75 \text{ m}$$

$$\therefore 0.75 = x \left[ \frac{13.6}{0.8} - 1 \right] = 2x.16$$

$$\therefore x = 0.466 \approx 0.05 \text{ m (corr 5 cm)}$$

Finding  
d in pipe  
in incl.

Find the discharge of water flowing through a pipe of 30cm diameter placed in an inclined position where a venturimeter is inserted, having a throat diameter of 15cm. The difference of pressure b/w the main & throat is measured by a liquid of sp.gra 0.6 in an inverted U-tube which gives a reading of 30cm. The loss of head b/w the main & throat is 0.2 times the kinetic head of the pipe.

Soln: Given:

$$Q = ?$$

$$d_1 = 30\text{cm} = 0.3\text{m}$$

$$d_2 = 15\text{cm} = 0.15\text{m}$$

$$S_o = 0.6$$

$$x = 30\text{cm} = 0.3\text{m}$$

$$h_L = 0.2 \times \frac{V_1^2}{g}$$

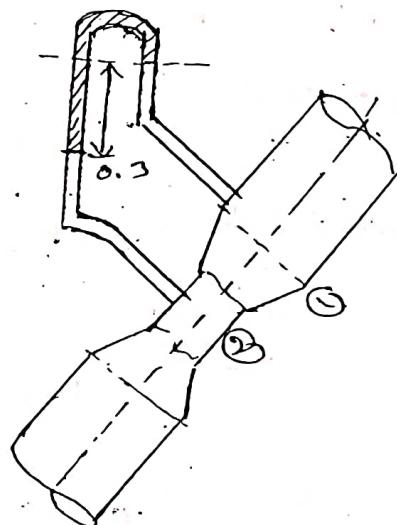
$$A_1 = \frac{\pi d_1^2}{4} = \frac{\pi (0.3)^2}{4} = 0.0706 \text{ m}^2$$

$$A_2 = \frac{\pi d_2^2}{4} = \frac{\pi (0.15)^2}{4} = 0.0176 \text{ m}^2$$

$$\text{U.K.T: } h = x \left[ 1 - \frac{S_o}{S} \right] = 0.3 \left[ 1 - \frac{0.6}{1} \right] = 0.12 \text{ m of H}_2\text{O}$$

Applying Bernoulli's eqn:

$$\therefore \frac{P_1}{\rho g} + z_1 + \frac{V_1^2}{2g} = \frac{P_2}{\rho g} + z_2 + \frac{V_2^2}{2g} + h_L$$



4) An orifice meter with orifice diameter 15 cm is inserted in a pipe of 30 cm  $\phi$ . The pressure difference measured by a mercury oil differential manometer on the 2 sides of the orifice meter gives a reading of 7 cm of mercury. Find the rate of flow of oil of sp. gravity 0.9 when the coefficient of discharge of the meter = 0.64.

Soln: Given -  $d_2 = 15 \text{ cm}$ ,  $d_1 = 30 \text{ cm}$ ,  $h = 7 \text{ cm of Hg}$ .

$$S_o = 0.9, C_d = 0.64$$

$$\therefore A_1 = \frac{\pi \times d_1^2}{4} = \frac{\pi \times (0.3)^2}{4} = 0.07 \text{ m}^2$$

$$A_2 = \frac{\pi \times d_2^2}{4} = \frac{\pi \times (0.15)^2}{4} = 0.02 \text{ m}^2$$

Differential head,  $h = x \left[ \frac{S_o}{C_d} - 1 \right]$

$$= 0.5 \left[ \frac{13.6}{0.9} - 1 \right] = 7.05 \text{ m of oil}$$

$$\therefore Q = \frac{C_d \times A_1 A_2 \sqrt{2gh}}{\sqrt{A_1^2 - A_2^2}}$$

$$= \frac{0.64 \times 0.07 \times 0.02 \sqrt{2 \times 9.81 \times 7.05}}{\sqrt{(0.07)^2 - (0.02)^2}}$$

$$\sqrt{(0.07)^2 - (0.02)^2}$$

$$Q = 0.15 \text{ m}^3/\text{sec}$$

A pitot static tube placed in the centre of 300 mm pipe line has one orifice pointing upstream and other perpendicular to it. The mean velocity in the pipe is 0.8 of the central velocity. Find the discharge through the pipe if the pressure difference b/w the 2 orifices is 60 mm of  $H_2O$ . Take co-efficient of pitot tube 0.98.

Soln:- Given:-  $d = 300 \text{ mm} = 0.3 \text{ m}$

$$V_{\text{mean}} = 0.8V$$

$$\alpha = ?$$

$$h = 60 \text{ mm of } H_2O = 0.06 \text{ m of } H_2O$$

$$C_v = 0.98$$

$$\text{U.K.T} \quad V_{\text{center}} = C_v \sqrt{2gh} = 0.98 \times \sqrt{2 \times 9.81 \times 0.06} \\ = 1.06 \text{ m/sec}$$

$$\therefore V_{\text{mean}} = 0.8 \times V_{\text{center}} = 0.8 \times 1.06 \\ = 0.85 \text{ m/sec}$$

$$\therefore Q = \text{Area of Pipe} \times V_{\text{mean}}$$

$$= \frac{\pi}{4} \times (0.3)^2 \times 0.85$$

$$= 0.060 \text{ m}^3/\text{sec}$$

6) Find the velocity of flow of an oil through a pipe when the difference of mercury level in a differential U-tube manometer connected to the tappings of the pitot tube is 80mm. Take co-efficient of pitot tube  $C_v = 0.98$ . & sp. gravity of oil is 0.8.

Soln Given

$$dL = 80 \text{ mm}$$

$$C_v = 0.98$$

$$S_o = 0.8$$

$$V = ?$$

$$\text{U.tube}, h = d \left[ \frac{S_m}{S_o} - 1 \right]$$

$$= 0.1 \left[ \frac{13.6}{0.8} - 1 \right]$$

$$h = 1.6 \text{ m of oil}$$

$$\therefore V = C_v \sqrt{2gh} = 0.98 \sqrt{2 \times 9.81 \times 1.6}$$

$$V = 5.49 \text{ m/sec}$$

7) A pitot tube is inserted in a pipe of 300mm  $\phi$ . The static pressure in pipe is 100mm of mercury (vacuum). The stagnation pressure at the centre of pipe, recorded by the pitot tube is 0.981 N/cm<sup>2</sup>. Calculate the rate of flow of water through pipe, if the mean velocity of flow is 0.85 times the central velocity. Take  $C_v = 0.98$ .

Soln Given,  $d = 300 \text{ mm}$

$$\text{Static pressure head} = -100 \text{ mm of Hg}$$

$$= -\frac{100}{1000} = -0.1 \text{ m} \times 13.6$$

$$= -1.36 \text{ m of Hg}$$

$$\text{Stagnation pressure head} = 0.981 \text{ N/cm}^2 = 0.981 \times 10^4 \text{ N/m}^2$$

$$\text{Stagnation pressure head} = \frac{P}{\rho g} = \frac{0.981 \times 10^4}{9810} \\ = 1 \text{ m}$$
(23)

$\therefore h = \text{Stagnation pressure head} - \text{Static pressure head}$

$$= 1 - (-1.36) \\ = 2.36 \text{ m}$$

$\therefore \text{Velocity at centre, } V = C_v \sqrt{2gh}$

$$= 0.98 \sqrt{2 \times 9.81 \times 2.36} \\ = 6.668 \text{ m/sec}$$

$$\therefore V_{\text{mean}} = 0.85 * V = 0.85 \times 6.668 \\ = 5.667 \text{ m/sec}$$

$$\therefore Q = A * V_{\text{mean}} = \pi \times \frac{(0.3)^2}{4} \times 5.667 \\ = 0.4 \text{ m}^3/\text{sec}$$

## The momentum Equation

It is based on the law of conservation of momentum or on the momentum principle which states that the net force acting on a fluid mass is equal to the change in momentum of flow per unit time i.e. in momentum of flow per unit time in that direction. The force acting on a fluid mass  $m$  is given by Newton's 2nd law of motion.

$$F = m \times a$$

But,  $a = \frac{dv}{dt}$

$$\therefore F = m \times \frac{dv}{dt}$$

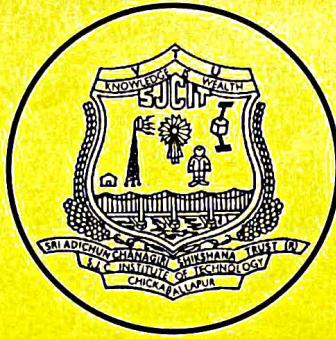
$$\boxed{F = \frac{d(mv)}{dt}}$$

( $\because m$  is constant known as the momentum principle)

It can also be written as,  $\boxed{\int F \times dt = d(mv)}$

Known as impulse-momentum equation. It states that the impulse of a force  $F$  acting on a fluid mass  $m$  in a short interval of time  $dt$  is equal to the change of momentum  $d(mv)$  in the direction of force.

II JAI SRI GURUDEV II  
SRI ADICHUNCHANAGIRI SHIKSHANA TRUST (R.)



**S.J.C. INSTITUTE OF TECHNOLOGY**  
CHICKBALLAPUR - 562 101.

*Assignment Book*

Name ..... ADNAN BAIG

Class ..... 3<sup>rd</sup> SEM. CIVIL ENG. Roll/Reg. No ..... Diploma

Subject ..... FLUID MECHANICS

Assignment No.	Date	REMARKS	Sig. of the Student	Sig. of the Staff Member
I				
II				
III	11/2/2022	ASSIGNMENT - III	10/10	Adn Baig 11/2/2022
IV	3/3/2022	ASSIGNMENT - IV	10/10	Adn Baig 03/03/2022

Staff in-Charge

Head of Department

**SJCIT CONSUMERS CO-OPERATIVE SOCIETY LTD.**

CHICKBALLAPUR - 562 101.

### Assignment - 03

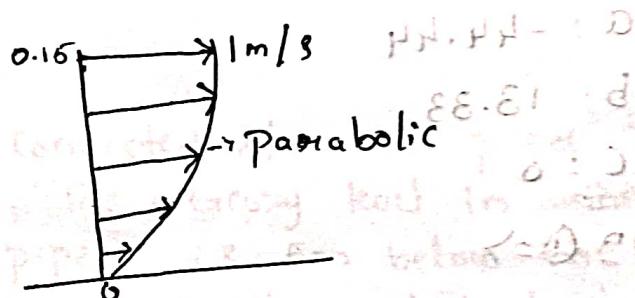
1. Calculate the velocity gradient of distance 0, 100, 150 mm from the boundary if the velocity profile is a parabola with vertex 150 mm from the boundary where the velocity is 1 m/s. also calculate the shear stresses of these points if the fluid is a viscosity of  $0.804 \text{ N} \cdot \text{s/m}^2$ .

$$\text{Soln: } M = 0.804 \text{ N} \cdot \text{s/m}^2$$

$$y = 0, 100, 150$$

$$U = 1 \text{ m/s}$$

$$y = 0, 0.1 \text{ m}, 0.15 \text{ m}$$



The velocity profile is given Parabolic, and the equation of velocity profile is

$$U = ay^2 + by + c \rightarrow ①$$

B.C

$$\text{at } y=0, U=0$$

$$\text{by } y=0.15, U=1$$

$$\text{c) } y=0.15 \quad \frac{dU}{dy} = 0$$

$$\text{at } y=0, U=0$$

$$U = a(0)^2 + b(0) + c$$

$$\boxed{c=0}$$

$$\text{by } y=0.15 \quad U=1$$

$$0.15 = a(0.15)^2 + b(0.15) + 0$$

$$0.0225a + 0.15b - 1 = 0 \rightarrow ②$$

$$\text{EE.81} + (0.0225) \text{PH. PH.} = 1.0 : \boxed{\frac{a}{b}}$$

$$\text{EE.81} + 0.0225 \cdot 1 = 1.0 : \boxed{\frac{a}{b}}$$

$$\text{EE.81} + 0.0225 = 1.0 : \boxed{\frac{a}{b}}$$

$$\frac{a}{b} = \frac{1.0 - 0.0225}{0.0225} = 44.44$$

$$c) y = 0.15 \quad \frac{du}{dy} = 0$$

so - boundary

$$\frac{du}{dy} = 2ay + b$$

$$2a(0.15) + b = 0$$

equation a & b

$$a = -44.44$$

$$b = 13.33$$

$$c = 0$$

$$\text{eqn } ① \Rightarrow$$

$$u = -44.44y^2 + 13.33y \rightarrow ②$$

differentiate w.r.t. y

$$\frac{du}{dy} = -44.44y + 13.33$$

i) velocity gradient

$$\left(\frac{du}{dy}\right)_{y=0} = -44.44(0) + 13.33 \\ = 13.33 \text{ s}^{-1}$$

$$\left(\frac{du}{dy}\right)_{y=0.1} = -44.44(0.1) + 13.33 \\ = 8.89 \text{ s}^{-1}$$

$$\left(\frac{du}{dy}\right)_{y=0.15} = -44.44(0.15) + 13.33 \\ = -6.666 + 13.33 \\ = 6.66 \text{ s}^{-1}$$

ii) Shear Stress

$$\tau = u \frac{du}{dy}$$

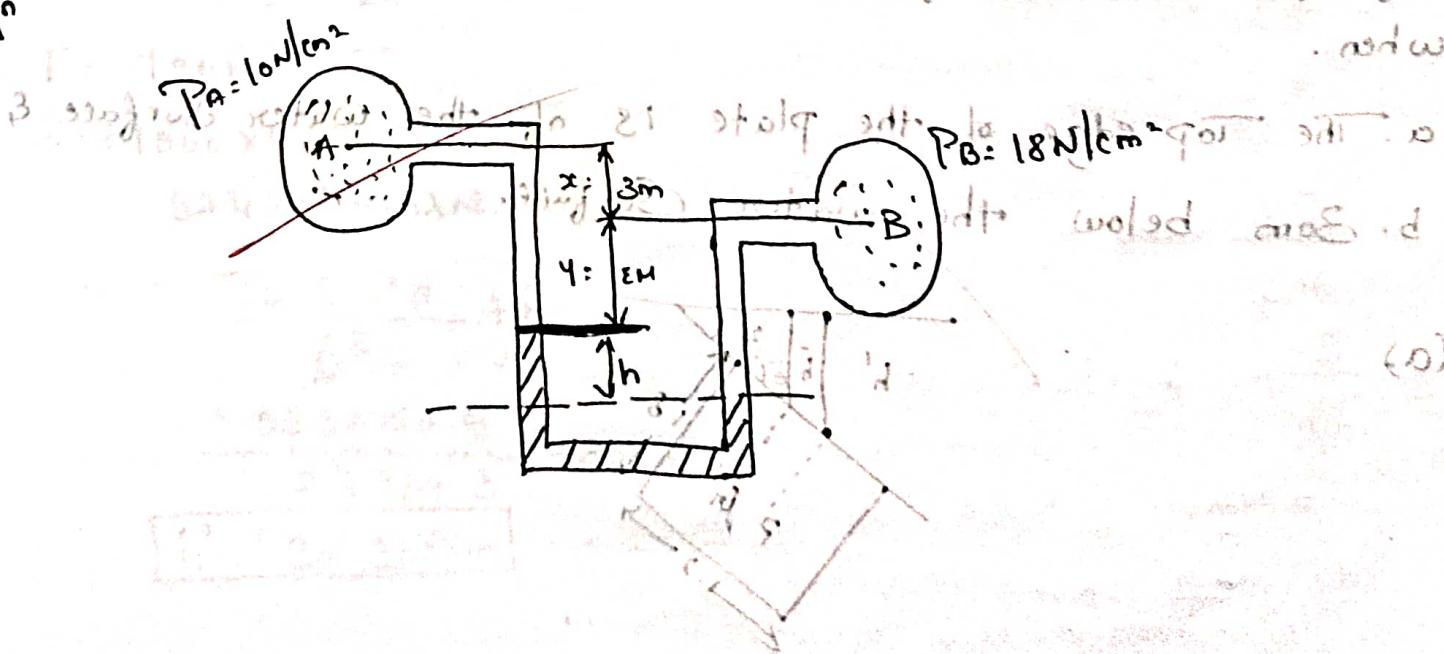
$$(\bar{\tau})_{y=0} = (0.804)(13.33) = 10.71 \text{ N/m}^2$$

$$(\bar{\tau})_{y=0.1} = u \frac{dy}{dy} = 0.804(8.18) = 7.147 \text{ N/m}^2$$

$$(\bar{\tau})_{y=0.5} = u \frac{dy}{dy} = 0.804(6.66) = 5.331 \text{ N/m}^2$$

2) A differential manometer is connected b/w two pipes A & B if pipe A is 3m above the pipe B. The mercury level in the manometer limb connected to the pipe A is 5m below the centre of the pipe A & is of a higher level than that of the limb connected to pipe B. The pipe A carries a liquid of specific gravity 1.3 & is maintained at a pressure of  $10 \text{ N/cm}^2$  while the pipe B carries a liquid of specific gravity 0.9. Determine the difference in mercury level in the differential manometer.

Sol<sup>n</sup>



$$P_A = 10 \text{ N/cm}^2$$

$$= \frac{10}{10^{-4}} \text{ N/m}^2$$

$$P_B = 18 \text{ N/cm}^2$$

$$= 18 \times 10^4 \text{ N/m}^2$$

$$T_a = 1.5 \times 1000$$

$$= 1500$$

$$T_b = 0.9 \times 1000$$

$$\gamma_a = 9800 \text{ N/m}^3$$

$$D = 3 \text{ m} \text{ at } h = 11.6 + 35.75 + 13.3416h = 18 \times 10^4 + 17658 + 8829h \text{ N/m}^3$$

$$y = 2 \text{ m} \text{ from } D \text{ and } 31.8 \text{ m } 39.9 \text{ depth of bottom} \text{ and } 30.8 \text{ m}$$

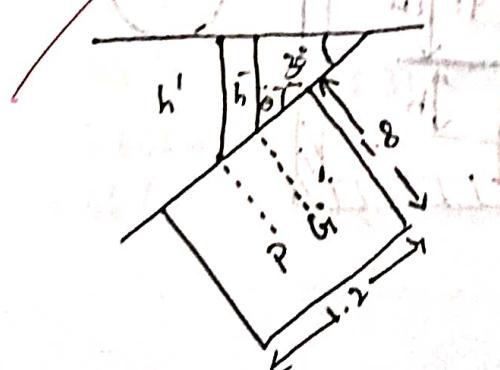
$$h_2 = 13.6 \times 1000 \text{ N/m}^3 \text{ water } 12452.7h = 24083 \text{ m } 39.9 \text{ depth } 30.8 \text{ m}$$

$$h = 13600 \text{ N/m}^3 \text{ water } 13600 \text{ N/m}^3 \text{ water } 0.1933 \text{ m}$$

3) A rectangular plate  $1.2 \text{ m} \times 1.8 \text{ m}$  size is immersed in water in an inclined position & makes an angle of  $30^\circ$  with the horizontal the  $1.2 \text{ m}$  side being horizontal. Calculate the magnitude of the force on one face & Position of centre of pressure when.

- The top edge of the plate is of the water surface &
- ~~30 m below the water surface.~~

(a)



$$h = 0.68 \sin 30^\circ$$

$$\bar{h} = 0.3$$

$$F = f g A \bar{h}$$

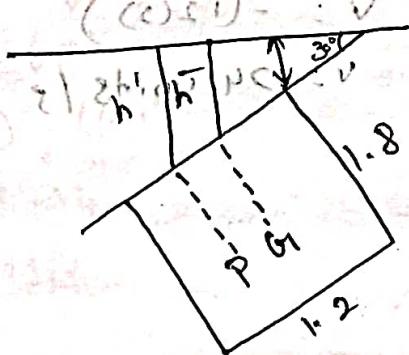
$$F = 1000 \times 9.81 \times 2.16 \times 0.3$$

$$F = 6356.88 N$$

$$h' = \frac{0.5832 \times 8 \sin^2(30)}{2.16 \times 0.3} + 0.3$$

$$h' = 0.525 m$$

by below 30m



$$\bar{h} = 30 + 0.6 \sin 30^\circ$$

$$\bar{h} = 30 + 0.3 = 30.3$$

$$F = f g A \bar{h}$$

~~$$= 1000 \times 9.81 \times 2.16 \times 30.3$$~~

~~$$= 6242044.88 N.$$~~

$$h' = \frac{16 \sin^2 \theta}{A \bar{h}} + h$$

$$= \frac{0.5832 \times 0.15}{2.16 \times 30.3} + 30.3$$

$$h' = 30.3022 m$$

$$I_n = \frac{bd^3}{12}$$

$$= \frac{12 \times (1.8)^3}{12}$$

$$= 0.5832 m^2$$

$$(d1 \cdot p \times c1) - \frac{P}{3c_6} = 0$$

$$(d1 \cdot p \cdot c1) - \frac{P}{3c_6} = 0$$

$$(d1 \cdot p \cdot c1) - \frac{P}{3c_6} = 0$$

$$2.16 \times 0.3 - \frac{P}{3c_6} = 0$$

$$0.5832 \times 0.15 - \frac{P}{3c_6} = 0$$

$$I \cdot (p \cdot c) + \frac{P}{3c_6} = 0$$

$$I \cdot (p \cdot c) + \frac{P}{3c_6} = 0$$

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$$I \cdot (p \cdot c) + \frac{P}{3c_6} = 0$$

4. If for a two-dimensional potential flow, the velocity potential is given by  $\phi = 4x(3y - 4)$ , determine the velocity of the point (2,3). Determine also the value of stream function  $\psi$  at the point (2,3).

$$\text{Sol}: \phi = 4x(3y - 4)$$

$$u = -\frac{\partial \phi}{\partial x}$$

$$u = -\frac{\partial}{\partial x} (12xy - 16)$$

$$u = -(12y - 16)$$

$$u = -(12(3) - 16)$$

$$u = -20 \text{ units/s}$$

$$v = -\frac{\partial \phi}{\partial y}$$

$$v = -\frac{\partial}{\partial y} (12xy - 16)$$

$$v = -(12x - 0)$$

$$v = -(12(2))$$

$$v = -24 \text{ units/s}$$

$$v = -20i - 24j$$

$$v = \sqrt{(20)^2 + (24)^2}$$

$$v = 31.24 \text{ units/s}$$

### Stream function $\psi$

$$\psi = -\frac{\partial \phi}{\partial y}$$

$$\frac{\partial \psi}{\partial y} = -4$$

$$\frac{\partial \psi}{\partial y} = 2y - 16 - 70$$

$$v = \frac{\partial \psi}{\partial x}$$

$$\frac{\partial \psi}{\partial x} = v$$

$$\frac{\partial \psi}{\partial x} = -12x \rightarrow \text{eqn } (2)$$

Integrate with respect to  $y$ .

$$\psi = \frac{12y^2}{2} - 16y + C$$

$$\varphi = 6y^2 - 16y + c \rightarrow ③$$

diff w.r.t. x

$$\frac{dy}{dx} = 0 - 0 + \frac{J_c}{J_s}$$

$$\frac{J_c}{J_s} = -12x$$

Integrate w.r.t. x

$$c = -\frac{12x^2}{2} + C$$

L is neglected

$$L = -6x^2$$

Substitute in eqn ③, contd.

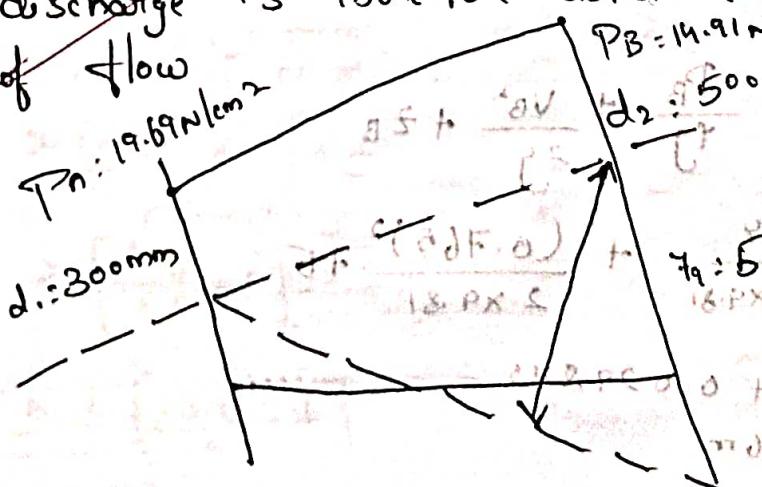
$$\varphi = 6y^2 - 16y = 6x^2$$

$$\varphi = 6(3)^2 - 16(3) = 6(2)^2 \\ : 16^2 - 48 - 24$$

$$\varphi = 90 \text{ units}$$

5) A pipe line carrying oil of specific gravity 0.8 changes in diameter from 300mm. to a portion of 400mm diameter to position B which is 5m higher level. If the pressure at A & B are  $19.62 \text{ N/cm}^2$  &  $14.91 \text{ N/cm}^2$  respectively & the discharge is 150 lit/sec determine the loss of head & direction of flow

Sol:



$$P_B = 14.91 \text{ N/cm}^2$$

$$h = 5 \text{ m} \times 10^3 \text{ N/m}^2 = 50000 \text{ N/m}^2$$

$\alpha \rho g \cdot 5 = \rho g \cdot 5 \text{ m}$  height of liquid

$$Q = 160 \text{ lit/sec}$$

$$Q = \frac{160}{1000}$$

$$Q = 0.16 \text{ m}^3/\text{s}$$

$$\text{Soil} = 0.8$$

$$P_a = 19.62 \text{ N/m}^2$$

$$P_a = 19.62 \times 10^4 \text{ N/m}^2$$

$$P_B = 14.91 \text{ N/cm}^2$$

$$= 14.91 \times 10^4 \text{ N/m}^2$$

$$Q = a_1 V_1$$

$$V_1 = \frac{Q}{a_1} = \frac{0.16}{0.04} = 1.142 \text{ m/s}$$

$$V_1 = \frac{Q}{a_2} = \frac{0.16}{0.196} = 0.765 \text{ m/s}$$

$$\text{Total head of A} = \frac{P_a}{\gamma g} + \frac{V_1^2}{2g} + Z_A$$

$$= \frac{19.62 \times 10^4}{1000 \times 0.8 \times 9.81} + \frac{(1.142)^2}{2 \times 9.81} + 0$$

$$= 19.97 + 0.233 + 0 = 20.203 \text{ m}$$

3. Head for 25.229 m total net loss

$$\text{Total head of B} = \frac{P_B}{\gamma g} + \frac{V_B^2}{2g} + Z_B$$

$$= \frac{14.91 \times 10^4}{0.8 \times 1000 \times 9.81} + \frac{(0.765)^2}{2 \times 9.81} + 0$$

$$= 18.998 + 0.029875$$

$$= 19.028 \text{ m}$$

flow from A to B

$$\text{loss of head: } T_A - T_B = 2.093 \text{ m}$$

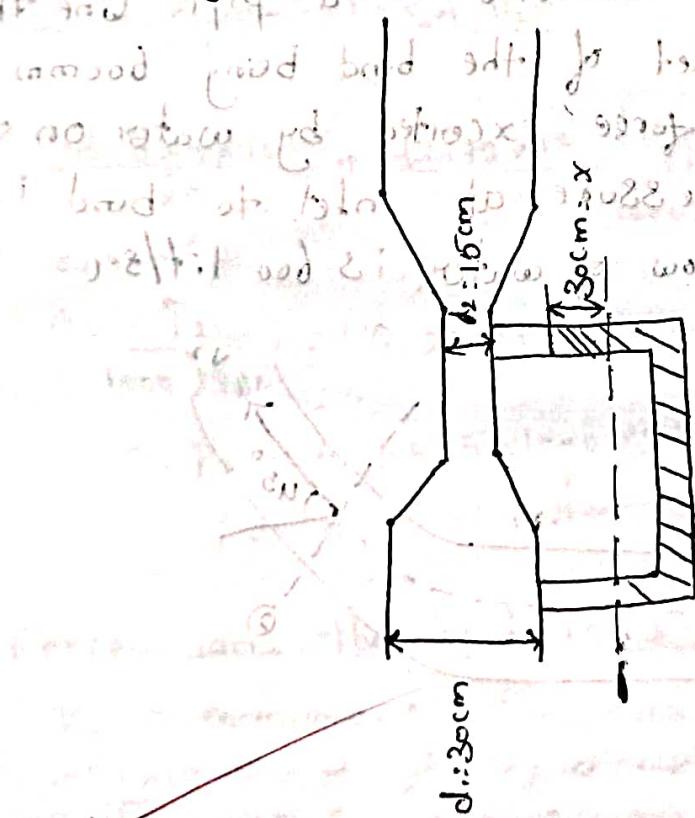
6) A  $30 \times 156$ m sec venturimeter is inserted in a vertical pipe carrying water, flowing in the upward direction. A differential mercury manometer connected to the inlet & throat gives a reading of 30cm. find the discharge. Take  $C_d = 0.98$

$$Sol^{\prime}: d_1 = 30\text{cm} = 0.3\text{m}$$

$$d_2 = 15\text{cm} = 0.15\text{m}$$

$$x = 30\text{cm} = 0.2\text{m}$$

$$C_d = 0.98$$



$$a_1 = \frac{\pi (0.3)^2}{4} = 0.0706\text{m}^2$$

$$a_2 = \frac{\pi (0.15)^2}{4} = 0.0176\text{m}^2$$

$$h = x \left[ \frac{h_m}{h_s} - 1 \right]$$

$$= 0.3 \left[ \frac{13.6}{2} - 1 \right]$$

$$= 3.78$$

$$Q = \frac{A_1 A_2 \sqrt{2gh}}{\sqrt{A_1^2 - A_2^2}}$$

$$= 0.98 \times 0.04 \times 0.01 \times \sqrt{2 \times 9.81 \times 3.78} \text{ m}^3/\text{sec}$$

$$\sqrt{(0.004)^2 - (0.00028)^2} = 0.1509 \text{ m}^3/\text{sec}$$

Q) A  $45^\circ$  reducing bend is connected in a pipe line the diameter at the inlet & outlet of the bend being 600mm & 300mm respectively. find the force exerted by water on the bend if the intensity of pressure at inlet to bend is  $8.829 \text{ N/cm}^2$  & rate of flow of water is 600 lit/sec.

Sol:

$$\theta = 45^\circ$$

$$D_1 = 600 \text{ mm}$$

$$= 0.6 \text{ m}$$

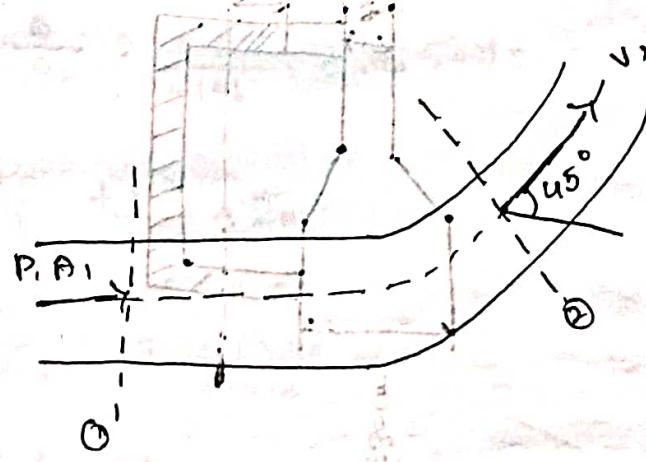
$$D_2 = 300 \text{ mm}$$

$$= 0.3 \text{ m}$$

$$P_i = 8.829 \text{ N/cm}^2$$

$$= 8.829 \times 10^4 \text{ N/m}^2$$

$$Q = 600 \text{ lit/sec} = 0.6 \text{ m}^3/\text{s}$$



$$A_1 = \frac{\pi}{4} D_1^2 = \frac{\pi}{4} (0.6)^2 = 0.1827 \text{ m}^2$$

$$A_2 = \frac{\pi}{4} D_2^2 = \frac{\pi}{4} (0.3)^2 = 0.07068 \text{ m}^2$$

$$V_1 = \frac{Q}{A_1} = \frac{0.6}{0.1827} = 3.29 \text{ m/s}$$

(1 - d/D) = 0.5

B.F.E.

$$V_2 = \frac{Q}{A_2} = \frac{0.6}{0.07068} = 8.488 \text{ m/s}$$

Applying Bernoulli's eqn of section ① & ② we get

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + Z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + Z_2$$

$$Z_1 = Z_2$$

~~$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} = \frac{P_2}{\rho g} + \frac{V_2^2}{2g}$$~~

$$\frac{8.829 \times 10^4}{1000 \times 9.81} + \frac{(2.122)^2}{2 \times 9.81} = \frac{P_2}{1000 \times 9.81} + \frac{(8.488)^2}{2 \times 9.81}$$

$$\frac{P_2}{1000 \times 9.81} = 9.2293 - 3.672$$

$$P_2 = 5.5575 \times 1000 \times 9.81$$

$$P_2 = 5.45 \times 10^4 \text{ N/m}^2$$

Force on the bend in x- & y direction are given

by equations

$$F_x = \rho g (V_1 - V_2) A_1 \cos 30^\circ + P_1 A_1 - P_2 A_2 \cos 30^\circ$$

$$= 1000 \times 0.6 [2.122 - 8.488 \cos 45^\circ] + 8.829 \times 10^4 \times 0.2828 - 5.45 \times 10^4 \times 0.07068 \times \cos 45^\circ$$

$$= -2327.9 + 24959.6 - 2720.3$$

$$= 24959.6 - 5048.2$$

$$= 19911.4 \text{ N}$$

$$F_y = 19 \left[ -V_2 \sin \theta \right] - P_2 A_2 \sin \theta$$

$$= 1000 \times 0.6 \left[ -8.488 \sin 45^\circ \right] - 15.45 \times 10^4 \times 0.07068 \times \sin 45^\circ$$

$$= -3601.1 - 2121.1$$

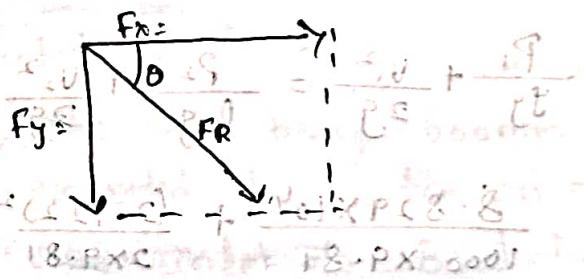
$$= -6322.2 \text{ N}$$

-ve sign means  $f_y$  is acting in the downward direction

$$\text{Resultant force } F_R = \sqrt{F_x^2 + F_y^2}$$

$$= \sqrt{(19911.4)^2 + (-6322.2)^2}$$

$$= 20890.9 \text{ N}$$



The angle made by the resultant force with x-axis is

$$\tan \theta = \frac{F_y}{F_x} = \frac{6322.2}{19911.4}$$

$$= 0.3145$$

$$\theta = \tan^{-1}(0.3145)$$

$$\boxed{\theta = 17^\circ 36'}$$

8) The head of water over an orifice of 100mm diameter is 10mm. The discharge through the orifice is 70 lps. If the coordinate of a point on the jet measured from vena contracta are 4.3 m horizontal & 0.5 m vertical, determined (d. Cu) & Cc.

$$d = 100 \text{ mm} \Rightarrow d/2 = 50 \text{ mm}$$

$$Q = 70 \text{ lps} \Rightarrow Q = d \cdot P \cdot D \cdot C_s \cdot C_d$$

$$Q = 64000 \text{ lps} \Rightarrow Q = d \cdot P \cdot D \cdot C_d$$

$$Q = 64000 \text{ lps} \Rightarrow Q = d \cdot P \cdot D \cdot C_d$$

Sol<sup>n</sup>:  $d = 0.1m$

$$a = \frac{\pi d^2}{4} = \frac{\pi \times 0.1^2}{4} = 853 \times 10^{-3} \text{ m}^2$$

$$x = 4.3 \text{ m}$$

$$y = 0.5 \text{ m}$$

$$\rho_{act} = \rho_0 [sec] = 0.07 \text{ m}^3/\text{sec}$$

$$Cd = \frac{\rho_{act}}{\rho_{the}}$$

$$= \frac{0.07}{0.1099} = 0.64$$

$$\rho_{the} = (\alpha \sqrt{2gh}) = 853 \times 10^{-3} \times \sqrt{2} \times 9.81 \times 10$$

$$\rho_{the} = 0.1099 \text{ m}^3/\text{sec}$$

$$Cd = \frac{\rho_{act}}{\rho_{the}}$$

$$= \frac{0.07}{0.1099} = 0.64$$

Wetterscheinung ist die Verteilung der Wärme im Raum.

$Cv = \frac{V_{act}}{V_{the}}$  (Volumenströmung ist ein Maß für die Verteilung der Wärme im Raum)

$$Cv = \frac{x}{2\sqrt{yH}} = \frac{4.3}{2\sqrt{0.5 \times 10}} = 0.961$$

$$Cc = \frac{Cd}{Cv} = \frac{0.64}{0.961} = 0.66$$

9. Water flows over a rectangular weir 1m wide of a depth of 150mm & afterwards passed through a triangular right angled weir. Taking Cd for the rectangular & triangular weirs as 0.62 & 0.59 respectively. Determine the depth over the triangular weir 801°.

$$l = 1\text{ m}$$

$$H_1 = 150\text{ mm} = 0.15\text{ m}$$

$$\theta = 90^\circ$$

$$Cd = 0.59$$

$$Cd_{\text{rect}} = 0.62$$

$$Q = \frac{2}{3} Cd \times l \sqrt{2g} [H^{3/2}]$$

$$Q_R = \frac{2}{3} \times 0.62 \times \sqrt{2 \times 9.81} (0.15)^{3/2} \\ = 0.1063 \text{ m}^3/\text{sec}$$

$$Q = \frac{3}{15} Cd \sqrt{2g} \tan \theta/2 [H^{5/2}]$$

$$0.1063 = \frac{3}{15} (0.59) \sqrt{2 \times 9.81} (1) [H^{5/2}] = 0.022$$

$$1.5945 = 0.84 [H^{5/2}]$$

$$\boxed{H = 0.3596 \text{ m}}$$

10. The rate of flow of water through a horizontal pipe is  $0.25 \text{ m}^3/\text{s}$ . The diameter of the pipe which is 200mm is suddenly enlarged to 400mm. The pressure intensity in the smaller pipe is  $4.77 \text{ N/cm}^2$ . Determine

- i) loss of head due to sudden enlargement
- ii) Pressure intensity in the large pipe
- iii) Power lost due to enlargement

$$Sol: \quad Q = 0.25 \text{ m}^3/\text{s}$$

$$d_1 = 200\text{mm} = 0.2\text{m}$$

$$d_2 = 400\text{mm} = 0.4\text{m}$$

$$P_1 = 11.77 \text{ N/cm}^2$$

$$P_2 = ?$$

$$a_1 Q = \frac{\pi d_1^2}{4} = \frac{\pi (0.2)^2}{4} = 0.031 \text{ m}^2$$

$$Q_2 = \frac{\pi d_2^2}{4} = 0.125 \text{ m}^2$$

$$Q = a_1 v_1 = a_2 v_2$$

$$V_1 = \frac{Q}{a_1} = \frac{0.25}{0.031} = 8.06 \text{ m/s}$$

$$V_2 = \frac{Q}{a_2} = \frac{0.25}{0.125} = 2 \text{ m/s}$$

i) Loss of head due to Sudden enlargement

$$h_e = \frac{(V_1 - V_2)^2}{2g} = \frac{(8.06 - 2)^2}{2 \times 9.81}$$

$$h_e = 1.81 \text{ m}$$

ii) Pressure intensity in large pipe

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + h_e$$

$$\frac{P_2}{\rho g} + \frac{P_1}{\rho g} + \frac{V_1^2}{2g} - \frac{V_2^2}{2g} - h_e$$

$$\frac{P_2}{1000 \times 9.81} = \frac{11.7 \times 10^4}{1000 \times 9.81} + \frac{(8.06)^2}{2 \times 9.81} - \frac{(2)}{2 \times 9.81} - 1.81$$

$$\frac{P_2}{1000 \times 9.81} = 11.9973.311 - 0.203 - 1.817$$

$$P_2 = 13.281 \times 1000 \times 9.81$$

~~$$P_2 = 13.02 \times 10^4 \text{ N/m}^2$$~~

~~10/16~~

~~10  
16~~

$$180.0 = \frac{f_{cR}}{P}$$

$$10.0 = \frac{f_{cR}}{P}$$

$$10.0 = P$$

$$10.0 = \frac{350}{16.9} = \frac{P}{10}$$

$$10.0 = \frac{350}{16.9} = \frac{P}{50}$$

temperature of water & sub base to 28.0 °C

$$18.0 = \frac{f_{cR}}{P}$$

$$18.0 = \frac{f_{cR}}{P}$$

18.0 = ~~10.0~~ ~~10.0~~

$$18.0 = \frac{f_{cR}}{P}$$

$$18.0 = \frac{f_{cR}}{P} = \frac{10.0}{10} = \frac{10}{10} = 10$$

$$18.0 = \frac{(10)}{16.9 \times 2} + \frac{(0.8)}{16.9 \times 2} + \frac{10 \times 10}{16.9 \times 2000} = \frac{10}{16.9 \times 2000}$$

# Internal Test Question paper format- CBCS Scheme

Name of the staff/s: Ankitha V, Ravindranath. C

Date: 09/10/2018

*Ankitha V 9/10/18*  
Signature: *Ravindranath 9/10/2018*

Reviewer's Signature: *9/10/18*

NOTE: Only the following information's to be given to the students.

## S.J.C. Institute of Technology

Department: Civil Engineering

Test: II

Subject Name: Fluid Mechanics

Semester: 3<sup>rd</sup>

Duration: 90 minutes

INSTRUCTIONS: Answer *any one* full question from each part.

Subject Code: 17CV33

Section: A & B

Max Marks: 30

Q.No.	Part-A	Marks	CO	Levels
1.	a) Comparison between i) steady & unsteady flow ii) Uniform & non-uniform flow.  b) The velocity potential function is given by $\Phi = 5(x^2 - y^2)$ . Determine the velocity component at the point (4, 5).  OR	05	CO3	L2
2.	a) Comparison between i) Laminar & turbulent flow ii) Path line & stream line.  b) A pipe line carrying oil of specific gravity 0.8 changes in diameter from 300mm diameter at position A to 500mm diameter at B which is 5m higher than A. If the pressure at A and B are respectively $20 \text{ N/cm}^2$ and $15 \text{ N/cm}^2$ and discharge is 150 lps, determine the loss of head.	05	CO4	L3
3.	Part-B  Derive an expression for Bernoulli's equation under energy principle.  OR	05	CO3	L2
4.	Derive an expression for continuity equation in Cartesian coordinates.	10	CO4	L3
5.	Part-C  A horizontal venturimeter with inlet and throat diameter 20cm and 10 cm respectively is used to measure the flow of water. The reading of differential manometer the inlet and throat is 20cm of mercury. Determine the rate of flow. Take $C_d = 0.98$  OR	10	CO5	L3

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6.	An orifice meter with orifice diameter 10cm is inserted in a pipe of 20cm diameter. The pressure gauges fitted upstream and downstream of the orifice meter gives readings of $19.62 \text{ N/cm}^2$ and $9.81\text{N/cm}^2$ respectively. Co-efficient of discharge for the meter is given as 0.6. Determine the discharge of water through pipe.	10	CO5	L3
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CO3=05M	CO4=15M	CO5=10M	L2=05M	L3=25M	L4=0M
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## Internal Test Question paper format- CBCS Scheme

Name of the staff/s: Ravindranath. C and Ankitha. V

Date: 12/09/2018

Signature: Ravindranath Ankitha  
12/09/18Reviewer's Signature: Review 12/09/18Review 12/09/18

NOTE: Only the following information's to be given to the students.

## S.J.C. Institute of Technology

Department: Civil Engineering

Test: I

Subject Name: Fluid Mechanics

Subject Code: 17CV33

Semester: 3<sup>rd</sup>

Section: A &amp; B

Duration: 90 minutes

Max Marks: 30

INSTRUCTIONS: Answer *any one* full question from each part.

Question Number		Marks	CO	Levels
1	a. Define the following fluid properties with units: i. Specific weight ii. Kinematic viscosity iii. Surface tension iv. Capillarity v. Dynamic viscosity.	5	CO1	L1
	b. A plate having an area of $0.6 \text{ m}^2$ is sliding down the inclined plane at 30° to the horizontal with a velocity of $0.36 \text{ m/s}$ . There is a cushion of fluid 1.8mm thick between the plane and the plate. Determine the viscosity of the fluid, if the weight of the plate is 280N.	5	CO1	L3
	<b>OR</b>			
	a. Distinguish between i. Cohesion and adhesion ii. Real and ideal fluid.	5	CO1	L1
2	b. Determine the minimum size of a glass tube for the capillary rise in it not to exceed 0.2mm of water. The surface tension of water in contact with air is $0.0725 \text{ N/m}$ and contact angle $60^\circ$	5	CO1	L3
	Calculate the velocity gradient at distances 0, 100, 150 mm from the boundary if the velocity profile is a parabola with vertex 150mm from the boundary where the velocity is $1 \text{ m/s}$ . Also calculate the shear stresses at these points if the fluid has a viscosity of $0.804 \text{ N-s/m}^2$ .	10	CO2	L3
	<b>OR</b>			
	a. Explain the different types of pressure. Give the relationship between them. Indicate these pressures by means of a sketch.	5		
	b. A hydraulic press has a ram of 300mm diameter and plunger of 45mm diameter. Determine the weight lifted by the hydraulic press when the force applied at the plunger is 500N.	5	CO2	L3



3	A U – tube differential manometer containing mercury is connected on one side to a pipe A containing carbon tetrachloride of specific gravity 1.6 under a pressure of 120 kPa and on the other side of a pipe B containing oil of specific gravity 0.8 under a pressure of 200kPa. The pipe A lies 2.5m above pipe B and the mercury level in the limb connecting with pipe A lies 4m below the pipe A. Determine the difference in the levels of mercury in the two limbs of manometer.	10	CO2	L3
	<b>OR</b>			
	Derive the expression for the vertical plane surface submerged in liquid	10	CO2	L3

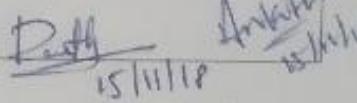
CO1=10M	CO2=20M	L1=05M	L2=00M	L3=25M
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**Internal Test Question paper format- CBCS Scheme**

Name of the staff/s: Ravindranath.C and Ankitha

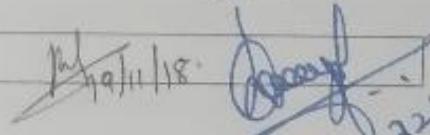
Date: 15/11/2018

Signature:



Ravindranath.C  
15/11/18

Reviewer's Signature:



Ankitha  
15/11/18



[Signature] 22/11/18

**S.J.C. Institute of Technology**

Department: Civil Engineering

Test : III

Semester:III Section: A &amp; B

Subject Name &amp; Code: FLUID MECHANICS

17CV33

**Instructions**

Duration: 90 minutes

Max Marks: 30

Q.No.	Questions	Marks	CO	Levels
1.	a) Derive an expression for Darcy Wishbech equation for frictional losses  OR	10	CO4	L4
	b) A closed cylindrical tank is 3.5m high and contains an oil of relative density 0.85 to a height of 3m above the bottom. The space above the oil surface contains air under a pressure of 50kN/m <sup>2</sup> . If an orifice of diameter 8 cm is provided on the side of the tank with its centre 25 cm above the bottom, estimate the weight of fluid discharge in one minute. Take Cd = 0.60	10	CO4	L4
2.	a) Determine theoretical discharge for Triangular notch  OR	10	CO5	L5
	b) A flow from a channel is controlled by a trapezoidal notch so that the full supply discharge of 2m <sup>3</sup> /s flows over the notch at a head of 1.2m measured over the crest. At half this head, a discharge of 0.6m <sup>3</sup> /s passes over the notch. Assuming Cd = 0.62, Determine the base width and side slope of notch.	10	CO5	L5
3.	a) Determine an expression for the discharge through a Venturimeter.  OR	10	CO5	L5
	b) A pipe line of 0.6m diameter is 1.5km long. To increase the discharge, another line of the same diameter is introduced parallel to the first in the second half of the length. Neglecting minor losses, find the increase in discharge if $4f = 0.04$ . The head at inlet is 300mm	10	CO5	L5

CO1=00	CO2=0	CO3=0	CO4=10	CO5=20	L1=0	L2=0	L3=	L4=10	L5=20
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# CBCS SCHEME

USN

18SJ17CV004

17CV33

## Third Semester B.E. Degree Examination, Dec.2018/Jan.2019 Fluid Mechanics

Time: 3 hrs.

Max. Marks: 100

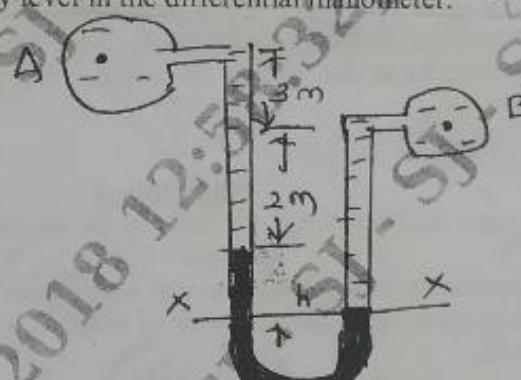
Note: Answer any FIVE full questions, choosing  
ONE full question from each module.

### Module-1

- 1 a. Define the term 'fluid'. Distinguish between liquid and gases. (06 Marks)  
b. Derive the expression for surface tension on a liquid droplet. (06 Marks)  
c. The dynamic viscosity of an oil, used for lubrication between a shaft and sleeve is  $0.6 \text{Ns/m}^2$ . The shaft diameter is 0.4m and rotates at 190rpm. Calculate the power lost in the bearing a sleeve length of 90mm. Take the thickness of the oil film as 1.5mm.  $P = \frac{1}{2} \rho \omega r^2 \times \pi d \times L \times h$  (08 Marks)

### OR

- 2 a. Explain the working of a Bourdon's pressure gauge with a diagram. (06 Marks)  
b. State and prove Pascal's law. (06 Marks)  
c. A differential manometer is connected at the two points A and B of two pipes as shown in Fig.Q.2(c). The pipe A contains a liquid of sp.gr = 1.5 while pipe B contains a liquid of sp.gr = 0.9. The pressures at A and B are  $9.81 \times 10^4 \text{ N/m}^2$  and  $17.65 \text{ N/m}^2$  respectively. Find the difference in mercury level in the differential manometer. (06 Marks)



$$h = -1.23 \text{ m}$$

### Module-2

- 3 a. Define: i) Total pressure ii) Centre of pressure. (04 Marks)  
b. Derive the expression for the total pressure and center of pressure on a vertically immersed plane surface. (08 Marks)  
c. The velocity potential function  $\phi = \frac{-xy^3}{3} - x^2 + x^3y + y^2$ .  
i) Find the velocity component in x and y directions.  
ii) Show that  $\phi$  represents a possible case of fluid flow. (08 Marks)

**OR**

- 4 a. Derive continuity equation in Cartesian coordinates for 3 dimensional flow. (08 Marks)
- b. A rectangular plane surface 1m wide and 3m deep lies in water in such a way that its plane makes an angle of  $30^\circ$  with the free surface of water. Determine the total pressure and the depth of center of pressure when the upper edge of the plate is 2m below the free surface. (06 Marks)
- c. What is flownet? The stream function for a two dimensional flow is given by  $\psi = 2xy$ . Find the velocity potential function ' $\phi$ '. (06 Marks)

**Module-3**

- 5 a. State the assumptions made in deriving the Euler's equation of motion. Hence obtain Bernoulli's equation from Euler's equation with a neat sketch. (10 Marks)
- b. A pipe of diameter 400mm carries water at a velocity of 25m/s. The pressure at the points A and B are given as  $29.43 \text{ N/cm}^2$  and  $22.563 \text{ N/cm}^2$  respectively, while the datum head at A and B are 28m and 30m. Find the loss of head between A and B. (05 Marks)
- c. Show that for a pitot tube actual velocity  $V = C_s \sqrt{y h}$  with usual notations. (05 Marks)

**OR**

- 6 a. Derive the equation for discharge through a venturimeter. (08 Marks)
- b. Water flow at the rate of  $0.147 \text{ m}^3/\text{s}$  through a 150mm diameter orifice inserted in a 300mm diameter pipe. If the pressure gauges fitted upstream and down stream of the orifice plate have shown readings of  $176.58 \text{ kN/m}^2$  and  $88.29 \text{ kN/m}^2$  respectively, find the coefficient of discharge 'C' of the orifice meter. (05 Marks)
- c. A  $45^\circ$  reducing bend is connected in a pipe line, the diameters at the inlet and outlet of the bend being 600mm and 300mm respectively. Find the force exerted by water on the bend if the pressure intensity at the inlet to the bend is  $8.829 \text{ N/cm}^2$  and rate of flow of water is 600 lit/sec. (07 Marks)

**Module-4**

- 7 a. Define hydraulic coefficient  $C_o$ ,  $C_v$  and  $C_d$  for an orifice and obtain the relation between them. (08 Marks)
- b. Derive the expression of discharge through a triangular notch. (08 Marks)
- c. Find the discharge over a Cipolletti weir of length 2.0m when the head over the weir is 1m. Take  $C_d = 0.62$ . (04 Marks)

**OR**

- 8 a. What are the advantages of triangular notch over rectangular notch? How do you classify mouth pieces? (06 Marks)
- b. A jet of water, issuing from a sharp-edged vertical orifice under a constant head of 10.0cm at a certain point, has the horizontal and vertical coordinates measured from the Vena-Contracta as 20.0cm and 10.5cm respectively. Find the value of  $C_v$ . Also find the value of  $C_c$  if  $C_d = 0.60$ . (06 Marks)
- c. What is broad crested weir? Show that under maximum discharge conditions  $h = 2/3 H$  with usual notations for a broad crested weir. (08 Marks)

**Module-5**

- 9 a. Derive Darcy's equation for head loss through pipes. (08 Marks)  
 b. Explain: i) Pipes in parallel ii) Pipes in series. (04 Marks)  
 c. The rate of water flow of water through a horizontal pipe is  $0.025 \text{ m}^3/\text{s}$ . The diameter of the pipe which is 200mm is suddenly enlarged to 400mm. The pressure intensity in the smaller pipe is  $11.772 \text{ N/cm}^2$ . Compute:  
   i) Loss of head due to sudden enlargement  
   ii) Pressure intensity in the large pipe. (08 Marks)

**OR**

- 10 a. Explain the terms:  
   i) Hydraulic gradient and  
   ii) Total energy line. (04 Marks)  
 b. Derive the expression for pressure loss due to sudden closure of the valve when the pipe is elastic. (08 Marks)  
 c. For a pipe network shown in Fig.Q.10(c) find the flow in each pipe. The value of 'n' mg/c assumed as 2.0. (08 Marks)

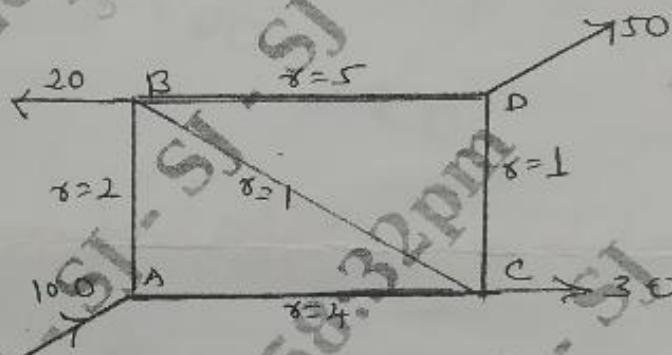


Fig.Q.10(c)